SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT

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SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT

1.0 INTRODUCTION

The South Fork (SF) Trinity River watershed in Trinity County (Figure 1) has been listed as a sedimentimpaired water-body in California's 1995 CWA 303(d) list, adopted by the State of California North Coast Regional Water Quality Control Board (NCRWQCB). This sediment impairment has, according to NCRWQCB, resulted in non-attainment of designated beneficial uses, primarily salmonid habitat. In December 1998, U.S. Environmental Protection Agency (EPA) established a Total Maximum Daily Load (TMDL) for sediment in the SF Trinity River watershed.

Implementation of sediment TMDL standards for a watershed with highly divergent sediment sources, due to differing bedrock geology and land management, such as the SF Trinity River, requires much more detailed information compared to less complex watersheds. Without specific information developed at a sub-watershed level, load allocations and reduction levels to meet specified targets are only crude estimates. Although the SF Trinity River has a considerable amount of existing information in many areas, a number of areas lack any appreciable data, and existing information does not allow refinement of source areas and allocations with any reasonable certainty beyond a main sub-watershed level.

In addition, the South Fork Trinity River Restoration Action Plan set a goal of the maintenance and restoration of anadromous salmonid populations in the watershed. Inherent in this over-arching goal is the need to assess conditions within the watershed and of the anadromous salmonid populations. Funds have been obtained from the California Fish & Game (SB 271) and State Water Resources Control Board (CWA 205(j)) to conduct two (2) years of data to support this assessment. The combined scopes of work envision fish populations (snorkel surveys), channel form, structure and substrate, sediment (collectively hydrologic and geomorphic monitoring) and temperature monitoring with a total budget of approximately \$225,000.

The purpose of this report is to compile, summarize, and analyze baseline hydrologic and sediment transport data for the SF Trinity River watershed that could be used for TMDL implementation and monitoring. This study combines office-based analyses of aerial photographs and GIS coverages with extensive streamflow, sediment transport, and geomorphic data collection.

1.1 WATERSHED OVERVIEW

The South Fork Trinity River basin is approximately 970 square miles in size, and is the largest tributary of the Trinity River. The terrain is predominately mountainous and forested, with only about 15 percent of the basin available for farmland, most of which occurs in the Hayfork Valley, the largest tributary of the South Fork. Elevations in the basin range from more than 7,800 feet above sea level in the headwater areas, to less than 400 feet at the confluence with the Trinity River.

The South Fork Trinity River has historically been recognized as a major producer of chinook and coho salmon and steelhead trout. The South Fork originates in the North Yolla Bolly Mountains about 50 miles southwest of Redding, and runs northwest for approximately 90 miles before reaching its confluence with the Trinity River near Salyer (Figure 1). The South Fork Trinity flows mostly through Trinity County, forming the boundary between Trinity and Humboldt Counties in its lower 12 miles. The

South Fork is the longest unregulated river in California. The 56-mile stretch from Forest Glen to the mouth is protected by the California Wild and Scenic Rivers Act.

Historically, the South Fork Trinity River was estimated to have total spawning escapements often over 10,000 fish. Anadromous species include chinook and coho salmon, steelhead trout, and Pacific lamprey (not a fish). A dramatic decline in numbers of anadromous fish was observed shortly after the large flood of December 1964, when a large flood event combined with poor land use practices relating primarily to timber harvest, and unstable geology led to unprecedented sediment delivery. Sedimentation from tributaries and inner gorge landslides completely overwhelmed the mainstem channel, causing channel change, filling pools, eliminating riparian vegetation and impacting spawning gravels. The degraded habitat limits the productive capacity of the river, and recovery from the 1964 flood and subsequent storm events has been slow.

2.0 SCOPE AND OBJECTIVES

The health and recovery of anadromous salmonids in the SFTR depend on a better understanding of instream conditions and associated long-term trends. The overall goal of this monitoring program is to provide landowners and land managers in the South Fork Trinity River Basin current data to assist in management decisions related to the implementation of the Sediment TMDL by the NCRWQCB and to assist land managers in their interactions with regulatory agencies. Hydrologic and geomorphic monitoring conducted in this study will assist in establishing baseline conditions, and form the basis for long-term trend monitoring of channel characteristics and sediment loads, with comparison to previous datasets where possible. Sampling will occur at locations throughout the SFTR basin.

In order to achieve these goals, the following general objectives have been developed:

<u>Objective 1: Pre-TMDL Implementation Plan base line</u>: This is a broad effort and must be conducted with the recognition that data will not identify sources of sediment. Instead this is an effort to provide data on sediment loads from the various geologic types within the South Fork Trinity River watershed recognizing that there are existing mixed uses in each.

- Collect and analyze sediment distribution data from approximately 15 sites throughout the watershed to provide a "snapshot" of conditions to measure future Implementation Plan and associated actions against, with the intent of using these data to [a] screen and refine more detailed sub-basin monitoring in the future and [b] sort baseline conditions by geology, with an understanding generally of the land management types and existing disturbances.
- At the present, funding for implementation of this monitoring plan and baseline assessment has allowed for two winters of data collection: Water Year 2002 (Oct 2001-Sept 2002) and Water Year 2003 (Oct 2002-Sept 2003). However, final reports to the funding agencies must be submitted by April and September 2003.

<u>Objective 2: Provide limited Sub-basin Effectiveness Monitoring</u>: This monitoring will involve the development of multi-station monitoring within selected sub-watersheds to facilitate adaptive management of various sediment reduction and restoration actions.

The activities undertaken as part of this project included the following specific short-term (current grant timeframe) implementation actions:

- 1) Review past and present monitoring efforts,
- 2) Identify reproducible past monitoring data,
- 3) Compile instream monitoring methods and protocols,
- 4) Reoccupy old sampling locations, as appropriate,
- 5) Establish new sampling sites, as required,
- 6) Install required monitoring equipment,
- 7) Collect hydrologic and geomorphic data for Water Years 2002 and 2003,
- 8) Analyze data,
- 9) Summarize data in water year reports, and compare to previous data where appropriate.

Long-term objectives of the SF Trinity Monitoring Program include:

- 1) Establish rating curves and/or relationships between water quality and quantity parameters at both a watershed and a site specific scale, enabling watershed-wide monitoring as well as BMP effectiveness monitoring,
- 2) Collect channel characteristic data (cross sections, profiles, bulk samples, pebble counts, residual pool volumes) every 5 years or after large flood events,
- 3) Document trends and changes in channel condition, and water quantity and quality,
- 4) Produce reports at appropriate intervals updating the results and trends of all monitored parameters.

As such, implementation of the Monitoring Program is a collaborative endeavor developed by a range of interested agencies, organizations, and individuals. As will be discussed later, the comprehensive work outlined in the Monitoring Plan is being implemented primarily by the US Forest Service and the Trinity County RCD. Coordination between these groups has resulted in the establishment of protocols that will provide comparable datasets.

Since this report is required to be prepared prior to the end of the sampling season, it cannot be comprehensive in scope, as considerable data remain to be analyzed. Instead, the data presented are intended to be illustrative of the overall methods used in this investigation. Likewise, although mention is made of the USFS monitoring program and elements, this report does not include any USFS data, with the exception of water temperature data.

3.0 DEVELOPMENT OF MONITORING PLAN AND QAPP

One of the first steps taken in this project was the development of a detailed hydrologic and geomorphic monitoring plan for the SF Trinity watershed. The plan was prepared in November 2001. Shortly thereafter, Quality Assurance Project Plans (QAPP) were developed for Surface Water, Channel Characteristics, and Sediment Laboratory Analysis. Since water temperature monitoring is being almost exclusively performed by the USFS at this time, a QAPP for that monitoring element was not prepared.

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4.0 METHODS

Introduction

The purpose of this section is to provide a succinct overview of field methodologies employed for streamflow and sediment transport monitoring, geomorphic reference reach establishment, and bulk sampling/permeability of spawning gravels. Detailed descriptions of these procedures are provided in the *Surface-Water Quality-Assurance Plan for the SF Trinity Geomorphic and Hydrologic Monitoring Project* (SWQA) and in the *Channel Characteristics Quality-Assurance Plan for the SF Trinity Geomorphic and Hydrologic Monitoring Project* (CCQA).

All field notes and data collection forms for all phases of this project were regularly photocopied and organized into notebooks by water year. All computer files and digital photographs are organized into a project file that is backed up to disks stored both on and off-site.

Site Selection

In order to characterize basin-wide hydrology and sediment production, thirty-four sites were chosen for streamflow and sediment transport monitoring on the basis of access, access permission, safety issues during storms and good channel hydraulics for gaging stations (Figure 1). Sub-basin areas ranged from a few acres (BTBV) to 379 mi² (HCHY) (Table 1). Most were located near culverts or bridges, though some (ECASFT, BCHC) were remote and required hiking or boat access. Some tributaries had multiple gaging stations (Barker Creek, Summit Creek, Rattlesnake Creek), while other stations (HCNH, HCHY, SFTFG) were located in large channels below major confluences.

The USFS established another 18 sampling sites, including three continuous recording stations (Figure 2). Four of these sites had sediment and streamflow data collected by TCRCD. No USFS discharge or sediment data are presented in this report.

4.1 SURFACE WATER MONITORING

4.1.1 Stage Measurement

At each of the 34 stations, a stage reference was established in a sheltered, low velocity area, upstream of a hydraulic control. Staff plates attached to channel iron driven into the streambed were installed at three of the study locations as stage measuring devices (HCNH, SFTFG, GCASFT). At the other 31 stations, river stage was measured from the water surface to the top of a fence post using a pocket surveyor's tape and initially recorded as a negative stage. All fence post tops were assigned a positive reference elevation (stage height correction factor) so the data could then be recorded in standard form: initial stage reading was added to the correction factor to create a positive river stage from the streambed to the water surface. The advantages of fence posts are: (1) low material cost, particularly when numerous stations are being installed, (2) simple, quick installation, and (3) low vandalism potential compared to more obvious staff gages.

Crest-stage gages, which allow measurement of the highest stage attained at a site during a given period, were installed at all sites. A pipe, perforated at its base, is securely attached to a fencepost or channel iron at a station, and finely ground cork is placed in the pipe which floats up as water rises and enters the pipe. The cork adheres, at the highest stage, to a wooden rod that had been placed inside the pipe. The cork line is read with a pocket surveyor's tape and initially recorded as a negative stage. The elevation of the

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crest-stage gage is surveyed into the site reference elevation to allow conversion of the crest-stage reading to the station gage height reading.

All stage references were surveyed to locally established benchmarks using an auto level. If sites were disturbed (by vandalism or high flows), the original gage datum could be re-established.

4.1.2 Continuous Stage Recorders

Continuous stage recorders (dataloggers) were installed at 15 stations in the South Fork Trinity River Watershed. The full site name, site acronym, associated watershed area, whether a datalogger was installed at the site, and whether a geomorphic reference reach was established, is shown in Table1.

All continuous stage recorder installations except one, utilized Global Water Level Loggers series #WL-15-15 or #WL-14-15. Due to manufacturing defects and subsequent malfunction, it became necessary to replace nine dataloggers during the study period. The other datalogger (at HCNH) is a Campbell Scientific CR10 with a Druck pressure transducer. This site was originally installed by the TCRCD in July 1996. Synthetic records were generated where possible to fill in missing periods of data. Global Water Level Loggers are of a pressure transducer type, utilizing a silicon diaphragm, and have a 15 foot range. Recording intervals were set to 15 minutes. Batteries were replaced and dataloggers were downloaded to a laptop computer on a regular monthly schedule. Gage height records were checked against observed values and adjusted to compensate for drift as necessary. Any error was distributed over the period of record between known (observed) gage heights.

All dataloggers were contained in locked steel gage houses anchored to trees or mounted to 4 x 6 inch posts set in 3 foot deep holes filled with concrete. Conduit from gage house to pressure transducer was provided by 1.5 or 2 inch galvanized pipe, either buried or tightly contoured to the slope profile, and clamped to t-posts. Photographs were taken of most gages (Figure 3). The original USGS gaging stations for South Fork Trinity at Forest Glen (USGS No. 11528100) and Hayfork Creek near Hyampom (USGS No. 11528500) were successfully re-occupied (Figure 4).

4.1.3 Streamflow Measurements

Direct streamflow discharge measurements were taken at all stations using standard or modified USGS methods. Most measurements were performed by wading at the gage location; however, high flow measurements were taken from bridges. One high flow measurement was performed with a boat and an Acoustic Doppler Profiler. Some very low flows were measured at culvert outlets using volumetric techniques.

In general, and when practical, standard USGS methods were used when making discharge measurements. During periods of rapidly changing river stage, however, fewer verticals were used in order to improve the accuracy of the measurement. Most discharge measurements contained 15-35 verticals. Stream flow equipment for wading included: 4 foot top-set wading rod, Keson 300 foot tape, JBS Instruments AquaCalc 5000-Advanced Stream Flow Computer, and either a Price AA or Pygmy current meter. Almost all measurements were performed with the magnetic head version of the Price AA or Pygmy meter. High flow measurements from bridges were made using a bridge-board, an A-reel, a Price AA meter, and a Columbus 50 lb. sounding weight.

The timing and magnitude of large-scale, infrequent floods, often precludes direct discharge measurement (Figure 5), as these peak flows often occur at night and substantial amounts of debris may also be present which can foul meters and make such measurements particularly hazardous. High flow measurements from bridges were typically collected during daylight hours on the falling limb of the storm hydrograph, after the debris load had declined. A peak discharge determined by indirect methods (slope-area) is often

the best means of defining the upper portions of the stage-discharge relation (rating curve). Because extrapolation of a rating curve beyond twice the highest measured discharge may be unreliable, discharge measurements for peak flood peaks made by indirect methods are preferable to rating curve extensions (Rantz and others, 1982, p.334).

Indirect discharge measurements for peak flows were computed at seven sites (HCNH, HCHY, SFTFG, SCWR, TCTCR, BTBV and GCASFT) using the slope-area method and the USGS Slope-Area Computation program. Crest gages installed on previously surveyed cross sections provided water surface slopes and cross section stage elevations during flood events (Figure 6). Roughness (Manning's n) values were assigned using one or more of the following techniques: solving for "n" at a known discharge, comparing field observations with published values (Barnes 1964, Hicks and Mason 1991), comparing derived values to reach specific n-values previously assigned by the USGS, and/or verification with the USGS NCALC program. At three sites (SCWR, BTBV and TCTCR), slope-area reaches were reconnoitered after peak flows and were surveyed for subsequent computations.

4.2 SEDIMENT TRANSPORT MONITORING

Sampling

Depth-integrated turbidity and suspended sediment sampling was performed at all locations. Sampling was performed using either a US DH-48 Depth-Integrating Suspended Sediment Sampler (for wadable flows) or a US DH-76 Depth-Integrating Suspended Sediment Sampler (rope-deployed from bridges at unwadeable flows). For the US DH-48, handles of different lengths were used depending on the flow depth. The US DH-76 is a rope-deployed sampler and is typically utilized from bridges. Sampling locations were located at or near stage locations. Standard methods, as developed by the USGS and described in Edwards and Glysson (1988) and in the SWQA, were generally used for sampling. However, due to the large number of sites being sampled, a tag line was not always set during sampling; instead distance between verticals was estimated. For each sample, the location, time, stage, number and duration of verticals, distance between verticals, bottle #, and whether a field replicate was taken, were recorded. At locations where it was not possible to get a true depth-integrated sample, grab samples or modified depth-integrated samples were taken and this information was recorded.

Samples were kept chilled after collection and stored in ice chests. Turbidity values were computed within 48 hours using a LaMotte 2020 turbidimeter. Suspended sediment concentrations were computed in the GMA sediment lab following USGS and ASTM D-3977 protocols. A laboratory QAPP was also prepared and submitted as part of this project.

4.3 GEOMORPHIC MONITORING

4.3.1 Geomorphic Reference Reaches

Site Selection and Monumentation

Six sites were chosen for geomorphic reference reaches, each of which was named according to the associated continuous recording station. Gaging station benchmarks and newly established benchmarks at the upstream and downstream ends of reaches were surveyed to the same datum. Stamped aluminum caps (atop a 5/8" rebar set in concrete) and monuments set by other agencies (such as the USGS reference marks at HCHY) were used as benchmarks and photographed (Figure 7). Level-loops of cross section endpoints and benchmarks were performed with an engineer's auto level to verify total station survey elevations. All surveys were checked for closure and held to a maximum error of 0.03 feet. Two-peg tests of the instrument were performed before each level-loop survey as per Harrelson et al. (1994).

Additional photo documentation was performed at each cross section. With a tape strung to identify the cross section, a field technician held a story board (indicating the cross section number) to one side of the body to describe a left bank or right bank view (Figure 6). Similarly, the story board was held overhead to indicate an upstream view, or below the waist to indicate a downstream view (Figure 8, bottom photo).

Channel Geometry: Cross Section and Longitudinal Profile Surveys

Surveys were conducted using field and documentation methods described by Harrelson et al. (1994). Cross section endpoints were installed on the left and right banks of the channel, well above bankfull stage and in locations not subject to washout, using four foot lengths of 5/8" diameter rebar. In some large channels, additional pins were set near the edge of water. For safety reasons, all rebar was driven deep enough that only a few inches were exposed, and then fitted with a secure plastic or aluminum cap. Pin elevations were surveyed with the caps on. Cross section numbers were stamped into caps and/or aluminum tags which were attached to the rebar. Six-foot fence posts driven five feet deep were used for endpoints in sandy areas.

Most cross sections were located at thalweg cross-over points (typically a riffle or a pool tail), because such areas provide greater resolution for evaluating channel change: pools do not typically store mobile coarse sediment. Each cross section was surveyed with a total station to obtain coordinate data for all cross section endpoints, used in the creation of site maps and allowing re-occupation even in the event of pin destruction. The left bank pin was generally set as Station "0", and all measurements were taken from left bank to right bank. Cross sections were oriented perpendicular to the high flow current vector. Survey points were taken at all slope breaks, generally at a minimum of 2 feet on center, along all cross sections. Approximate bankfull stage elevations, crest gage elevations, obvious high water marks, and abrupt changes in roughness elements (for slope-area computations) were surveyed on each cross section.

All longitudinal profile reach lengths exceeded the minimum of 25 times the width of the active channel as specified in the Channel Characteristics QAPP (CCQA). Longitudinal profiles of the thalweg were surveyed using a total station and prism pole, since it is nearly impossible to accurately stretch a tape down a meandering channel. The total station records angles and distances between survey shots. The longitudinal profile surveys were measured along the entire length of each reach, and recorded all pools, riffle crests, and slope changes. The distance between consecutive survey points was a function of grade change and the size of the channel, as smaller channels require more closely spaced survey points. However, distance between consecutive points did not exceed one-third of the active channel width.

Channel Characteristics: Substrate

Surface particle counts were conducted along the cross sections following methods described by Wolman (1954), modified for the use of a portable sampling frame (Bunte and Abt 2001). Each of the 100+ particles for each count was obtained from the intersection of the wire intercepts on the frame and then measured using a "gravelometer" template with square openings. The pebble counts were entered as the number of particles retained in each sieve class, for subsequent conversion to the cumulative percentage (by number) finer than the corresponding sieve size. Surface particle count results were entered in the project field book at the sampling location. On cross sections with multiple homogeneous sub-populations (facies), more than one particle count was conducted.

Channel Characteristics: The V* Method

 V^* is a method for assessing substrate quality that measures the fraction of residual pool volume impacted with fine sediment (usually fine sand to medium gravel) (Hilton and Lisle 1993). This fraction (V*) is the ratio of fine sediment volume to pool water volume plus fine sediment. Residual pool volumes were calculated from (1) depth soundings to the top/bottom of the sediment layer along cross section transects (Figure 8 – top photo), and (2) the difference in depth (bed elevation) between a pool and the downstream riffle crest. At least three riffle crests depths were taken with a graduated rod. The depth of fine sediment was measured by driving a 1.5 cm graduated metal probe into the fine graded sediment portion of the pool until coarser sediment was felt. Six to twenty soundings were taken along four to ten transects in all pools along the surveyed longitudinal profile. Sampling intensity was adjusted meet to the complexity of the scenario encountered: fewer soundings were taken in simple pools with no fine sediment.

4.3.2 Bulk Sampling and Permeability of Mainstem Spawning Gravels

Site Selection and Establishment

Three South Fork Trinity River mainstem sites were chosen: one near Forest Glen (SFTFG), one in Hyampom upstream of the Hayfork Creek confluence (SFTHR), and one below the Hayfork Creek confluence near Eltapom Creek (SFTEC). SFTFG overlapped an existing geomorphic reference reach. Sampling sites were chosen in accordance with well-documented criteria for spawning habitat site selection by anadromous salmonids (Bjornn and Reiser 1991). Within a week of completion, chinook salmon (*Oncorhynchus tshawytscha*) were observed spawning within a few feet of chosen sampling locations at SFTHR and SFTEC.

For each site, a monumented cross section was established using 5/8" rebar on each bank as endpins. Cross sections and associated benchmarks were surveyed with a total station. Bulk sample locations along the cross section were randomly determined and surface particle counts were obtained prior to sampling. A tape was strung between endpins to precisely locate the sample site along each cross-section. Each site was photographed (Figure 9).

Bulk Sampling

Either a 1.5 or 2 foot diameter McNeil type sampler was used. Two samples per cross section were taken by working the samplers into the gravel bed. The surface layer, defined as the depth of the largest surface particle (intermediate axis), was kept separate from the subsurface component of each sample. Most surface samples consisted of a single bucket, to be analyzed separately. The remaining bed material was transferred to buckets until the hole was excavated to a depth of 1.0 feet, the assumed typical egg-pocket depth for chinook salmon (Bjornn and Reiser, 1991). The excavated sample material was then dried in the field, on large tarps spread out in full exposure of the sun.

A Gilson TS-1 sample processor and generator were transported into the field on a trailer for shaker-sieve processing. However, the motor failed while processing the first sample and all samples had to be transported to the lab for processing. All bed materials down to 45 mm in diameter were hand-processed and weighed in the field using the "gravelometer" template and an Ohaus Model FG-30K digital scale.

Permeability

Permeability is a measure of the ability of a porous medium to pass water and as such, is a characteristic of spawning gravels that directly influences the delivery of oxygenated water to, and the removal of wastes from, developing salmonid embryos. Intragravel permeability was measured at no less than four locations adjacent to each bulk sampling location using a modified Terhune (1958) method with a backpack electric pump (Figure 9). An additional measurement of permeability was taken within each of the bulk sample locations. Five replicate measurements were taken at each of the five sample points (one measurement point in the center of the sampling location, four around the outside). The permeability standpipe was driven into the gravel until the bottom of the perforated portion was 35 cm below the bed surface. A permeability rate was calculated by recording the time required to fill the cylinder with a measured volume of water.

4.4 WATER TEMPERATURE

Only one water temperature station has been maintained by TCRCD since 2000, that of Hayfork Creek near Hayfork. This site has been in operation since July 1996. Prior to 1998, the TCRCD in conjunction with NRCS, USFS, and Timber Products Company had maintained a network of temperature gages (Figure 10) (Farber et. al.1998).

4.5 GIS

GIS coverages were obtained from a variety of sources including U.S. Forest Service and Trinity County. Existing road networks based on USFS and Trinity County datasets were supplemented by examination of the 1994 orthophoto quads. Harvest areas were determined from USFS plantation coverages and then updated for private lands by mapping from the 1994 orthophoto quads.

INTRODUCTION

Datalogger failures precluded sediment and discharge computations for some stations. Continuous streamflow data (15 minute hydrographs) were computed for ten stations exhibiting adequate and appropriate records. Suspended sediment load computations were performed for these 10 stations. Synthetic hydrographs were generated to facilitate sediment load computations for five manual stations in the Barker Creek watershed, discussed separately. Twenty-eight stage-discharge rating curves were developed for stations with sufficient measurements to define the relationships (Appendix A). Turbidity versus suspended sediment load versus discharge (Appendix C) and suspended sediment load versus discharge normalized by watershed area (Appendix D) for 23 stations.

The following were completed for the geomorphic and bulk sampling components of this study: site maps, long profile charts, cross section charts, particle size distributions (from pebble counts and bulk samples), permeability analyses, V* analyses, and photo documentation.

5.1 STREAMFLOW

5.1.1 Discharge Measurements and Peak Discharges

A total of 253 discharge measurements were taken from WY 2001 to WY 2003 (Table 2). Peak discharges were obtained from known stage heights by either (1) extending the rating curve, or (2) computing a slope-area estimate (Table 3). The December 16, 2002 peak discharge at HCNH exceeded the January, 1997 peak, as evidenced by stage observations during both events. All discharge measurements were entered and cataloged using the standard USGS-type 9-207 discharge measurement summary form (Table 4).

5.1.2 Rating Curves

Stage/discharge relationships (rating curves) were developed for 28 sites. Stage/discharge pairs were plotted on standard rating paper (USGS-type 9-279-M) and a best-fit line was hand drawn following standard USGS procedures, for four of the sites presented in this report (HCHY, HCNH, BCSR and SFTFG) (Figure 11). Hand plotted ratings tend to be more accurate, since few gaging sites have an entirely linear relationship between stage and discharge. For most stations, the Excel generated regression trendline ($r^2 > 0.99$) was used and no hand plot was drawn (Figure 12), as the more laborintensive hand techniques would not likely improve the results. Skeletal rating points were then extracted from the best-fit lines to develop rating tables (used in subsequent hydrograph generation and sediment load computations). Surface Water, a software package developed by Western Hydrologic Systems, was used to automatically expand rating tables from the skeletal points. Rating tables are: (1) used by the Surface Water program internally to compute annual discharge summaries, (2) converted to a vertical record for sediment and discharge computations, and (3) formatted into an Excel table for use by field personnel (Table 5).

5.1.3 Hydrographs

Once developed, the rating tables were used to determine the discharge for all stages in the continuous gaging records (15-minute gage height intervals) retrieved from the dataloggers. This technique assumes the hydraulic control remains stable throughout the hydrograph period, especially during storm events; e.g. the control does not scour, nor does it become artificially elevated by the accumulation of large

woody debris. Figure 13 illustrates the series of large storms in December 2002 and two smaller storms in January and March 2003. The shapes of the other site hydrographs are quite similar.

When datalogger failure resulted in missing periods of record, synthetic records were generated using a nearby station record: discharge values (computed from a wide range gage heights when both gages were operating) were plotted against one another, and the resulting regression was used to compute the missing flow record. This method proved more accurate than others, including percent basin area relationships and the use of separate regression equations for periods of rise and fall. Synthetic records were checked against observed gage heights and adjusted if necessary. Synthetic records are indicated as such on printed hydrographs (Figure 14).

5.2 SEDIMENT TRANSPORT

5.2.1 Turbidity and Suspended Sediment Concentration Measurements

A complete summary for ten datalogger sites is given in Table 6. Suspended sediment concentration (SSC) and turbidity were computed for depth-integrated samples, while only turbidity was computed for grab samples. A summary of all turbidity measurements from WY 2001 to WY 2003 is given in Table 7. Samples that did not meet the criteria outlined in the SWQA were not included in subsequent sediment load computations.

Suspended sediment and turbidity relationships were developed for the entire watershed as a whole and for each site individually. Individual site relationships developed included: SSC versus turbidity, turbidity versus discharge, SSC versus discharge, and suspended sediment load versus discharge. The equations and R^2 values (based on simple linear regressions) developed for each of these relationships are shown in Table 8.

All data were combined to develop the relationship between SSC and turbidity for the entire South Fork Trinity River Watershed (Figure 15). For the ten datalogger sites included here, relationships for suspended sediment load versus discharge are shown collectively (Figure 16), and by individual station (Appendix C). Discharge was normalized by watershed area to develop individual relationships for comparison by site (Appendix D), and between sites (Figure 17). Finally, total suspended sediment load for each site was plotted against drainage area (Figure 18).

5.2.2 Suspended Sediment Loads

Suspended sediment loads were computed from the regression equations (Table 8) and the 15 minute discharge hydrographs for WY 2002 and WY 2003 through July 1. Accuracy of load values derived from this type of analysis is dependent upon the number of samples and the range of discharges sampled at each station. Some sites, such as HCHY, clearly require more samples at higher discharges. The maximum observed turbidity at HCHY (499 NTU) was obtained from a grab sample by a volunteer during the highest observed discharge during the study period, the December 16, 2002 storm. Had this volunteer been able to take a depth integrated sample, the relationship between suspended sediment concentration and discharge could have been more accurately defined, increasing confidence in annual load estimates for this station.

In the first (April) version of this report, Summit Creek (SCWR) had discharge measurements performed up to 178 cfs, which predicted a peak of 1660 cfs. In order to better develop the high end of the rating curve, a slope area survey was completed April 3, 2003 for the peak flow on March 15, 2003. The water surface slope was marked for a stage height/discharge within the known rating (112 cfs), and this value was used to solve for Manning's n (n = 0.15). This high roughness value is confirmed by field

observations: Summit is steep, bedrock controlled, with mid-channel vegetation. The n-value for the peak flow (GH = 3.19 ft) was reduced to 0.12 to account for the greater than 1 foot increase in depth. This method produced a discharge of 334 cfs (Figure 12). The updated discharge rating predicts a peak WY 2003 discharge of 1430 cfs. This rating was used to re-compute WY 2002 and 2003 discharge and sediment load records for SCWR.

Also since the last report, another high flow measurement was performed at Tule Creek for the April 19, 2003 storm (244 cfs). Additionally, three slope area measurements were computed for: a known discharge of 140 cfs, and for stage heights of 3.62 and 4.88 feet. The known value was used to solve for Manning's n (0.065), which was reduced to 0.60 for the peaks to compensate for diminishing roughness with increased depth. An inflection was observed in the rating, which corresponds to the point where Tule Creek encounters a different channel configuration than at low flows (Appendix A-13). Tule Creek may exhibit yet another change in its stage-discharge relation at a higher flow (Figure 19), but until more flow measurements are taken at higher flows, this high flow rating must suffice. The R² values exhibited by the new Excel-generated ratings preclude the need for a hand plot. Sampling during the March 15, 2003 storm, coupled with the new discharge rating, resulted in the reduction in predicted load total reported here versus the first report (Table 9).

Grouse Creek is the most isolated site and is not always accessible during storms. For this reason, a slope-area reach was established to facilitate peak discharge estimates. Twelve meter measurements were performed up to 691 cfs and this value was used to solve for Manning's n (0.066), which was reduced to 0.055 for the December 28, 2002 peak flow of 5800 cfs (Figure 19). A shift was observed in the low flow discharge rating from WY 2002 to WY 2003 (Appendix A-26). Both ratings were extended with slope-area estimates. The exact time of the shift could not be determined (the high degree of disturbance adjacent to the stream in the fall of 2002, from road construction activities, could not be ruled out as a potential factor), so the ratings were applied to their respective water years. On December 16, 2002, Grouse Creek experienced the second highest peak during the study period (5400 cfs). If this event caused the shift, any error introduced from applying the 2003 rating to the period from October 1 to December 16, would be minimal as evidenced by the hydrograph (Figure 20).

Eltapom Creek (ECASFT) is another isolated site. Field personnel must cross the mainstem of the South Fork (which is usually over 10,000 cfs during storms) to sample Eltapom. Consequently, only four samples were collected and discharge measurements were only performed up to the wading limit.

Given the relatively small number of samples, specific site sediment relationships for intra-storm time or stage trends (hysteresis – variability in sediment transport rates based on hydrograph position, such as rising and falling stage), though frequently observed in sediment transport studies, were not usually examined here. Often, computations of transport records, that do not consider such hysteresis, may lead to considerable errors.

5.3 GEOMORPHIC MONITORING

Geomorphic Reference Reaches

Data collected at geomorphic reference reaches provide a "snapshot" of existing channel conditions, which becomes increasingly relevant as measurements are repeated over time, especially following large flood events. A complete summary of geomorphic parameters obtained for each of the six sites is given in Table 10. Previous work (by the USGS and USFS) will allow evaluations of channel change at some sites.

Since surveys were done with a total station, cross section and longitudinal profile data were used to generate site maps (Appendix E). All longitudinal (thalweg) profile reach lengths exceeded the minimum of 25 times the width of the active channel (CCQA) (Appendix F). Cross-sections were used not only for baseline descriptions of channel geometry, but as a key component for hydraulic modeling techniques such as the slope-area method (Appendix G). Particle size distributions were computed for 58 pebble counts in the geomorphic reference reaches (Table 11). The geometric mean (D_{mean}) may be the most useful comparator between sites, as it is the single-value parameter that describes the entire distribution. The D_{84} for wet channel pebble counts may provide a useful descriptor of spawning habitat parameters, as most cross sections traversed pool-tail type features. Bar-top pebble count D_{50} may provide an index for evaluating channel storage parameters over time. The WY 2003 peak flows would justify repeating pebble counts and channel surveys at the geomorphic sites. Site photographs are stored in digital files and may be useful for qualitative comparisons after a substantial geomorphic event.

5.3.1 Hayfork Creek near Hayfork (HCNH)

The longitudinal profile extends from just downstream of the Tule Creek confluence nearly a mile to the Mercil Bridge (Appendix E-1). All cross sections (except Cross Section 3, the gaging section) were surveyed across riffles or pool tails (Appendix G-1). Two new concrete benchmarks were established at the upstream end of the reach and surveyed to the original gage reference elevation. A prominent bedrock outcrop near the Mercil Bridge, and the bridge foundation itself, were used as reference elevations at the downstream end. A galvanized crest gage was installed at the bridge to obtain water surface slope profile for the entire reach during peak flows.

The lower portion of this reach is heavily used for grazing by cattle, which were actively using the stream at the time of data collection. While the data for V* have not been computed as of this draft report, qualitative observations suggest an increase in the volume of sediment stored in pools adjacent to grazing areas. This may demonstrate the local effects of bank erosion from cattle use, and not an overall trend in fine sediment storage for Hayfork Creek.

5.3.2 Butter Creek above South Fork Trinity (BUCSFT)

Four of the surveyed cross sections were included in the longitudinal profile length, which begins approximately 0.9 mile above the confluence with the South Fork Trinity (Appendix F-2). The other two represent re-occupied USFS cross sections (surveyed in 1989 and 1992) downstream of the geomorphic reach (Appendix G-2). All cross sections, including the original USFS cross sections, were photographed. Aluminum caps in concrete and gage structures were used as benchmarks.

5.3.3 Grouse Creek above South Fork Trinity (GCASFT)

The reference reach for Grouse Creek extends from the USFS Route 6 bridge down to the cascade created by Devastation Slide. A large volume of sediment is stored above the slide, through which Grouse Creek meanders unconfined. To accommodate slope-area observations, the four cross sections were located in the steeper, more confined segment, from the bridge down to the beginning of the alluvial deposit above the slide (Appendix G-3). More cross sections and a longer profile are required to monitor changes in sediment storage above the slide, and changes to the slide cascade.

Aluminum caps in concrete, bridge structures, and the large boulder used in previous surveys, were used as benchmarks. In August, 1997, the USFS (Six Rivers NF) surveyed three cross sections and a longitudinal profile of 4680 feet, from the bridge to the bottom of the cascade created by the slide. No USFS cross section pins could be located.

5.3.4 Hayfork Creek in Hyampom (HCHY)

The longitudinal profile for HCHY extends from the gage site (Cross Section 1), nearly one mile to the

riffle below the Hyampom Road Bridge (Appendix E-4). As previously described, HCHY is a reoccupation of the original USGS gage near Hyampom (Figure 4). Both of the original USGS (brass cap) reference marks were used as benchmarks (Figure 7). Since the original USGS gage datum was obtained from the 2002 survey, USGS stage/discharge relations can be compared. Using the original USGS high flow measurement data may allow changes to Cross Section 2 to be evaluated: it is located directly beneath the original USGS cableway. Further, original slope-area survey notes, which have been requested from USGS archives, may facilitate an evaluation of changes to the longitudinal profile (Appendix F-4).

5.3.5 Pelletreau Creek at Hyampom Road (PCHR)

The geomorphic reach on Pelletreau Creek begins below the last major bedrock constriction above the highly aggraded (1964 flood) alluvial plain visible from the Hyampom Road Bridge (Appendix E-5). The stream channel above the bridge is highly unstable, often braided, other times confined against one side of the valley by the accumulation of stored sediment, cutting into the erodible valley wall, causing bank erosion and landslides. Below the bridge, the channel becomes even less stable, migrating within the alluvial plain. Changes to the longitudinal profile near the gage are evidenced by a shift in the rating curve after the January 1997 storm (Appendix A-23).

Two concrete benchmarks were established near the bridge, and a scribe on the bridge pier (with an elevation painted next to it) was surveyed. The USFS surveyed six cross sections and a long profile each year from 1989 to 1991, and again in 1993 and 1997. Five of these cross sections were successfully reoccupied, and new rebar pins were installed at endpoints (Appendix G-23 through G-27). All USFS sketch maps of pin locations were repeated. Some of the original USFS photo points were repeated. The USFS surveys were compared to the 2002 surveys to evaluate changes to the cross sections and longitudinal profile. Potentially, using the thalweg depths in pools as a datum (where Pelletreau has cut down to bedrock), changes to the volume of sediment stored in the reach upstream of the bridge could be computed.

Since V^* requires a water surface for a reference, and since most of the stream flowed sub-surface at the time of survey, V^* was not performed. An irrigation diversion in the cascade above the reach diverts a substantial amount of the flow. Hundreds of juvenile salmonids were observed trapped in the warm, shallow pools below this diversion.

5.3.6 South Fork Trinity at Forest Glen (SFTFG)

The original USGS gaging site, and the current gage, is located approximately in the middle of this reference reach (Appendix E-6). The longitudinal profile begins 3000 feet upstream of the Highway 36 Bridge and ends approximately 1800 feet below the bridge (Appendix F-6). Caps in concrete, USFS concrete structures, and a state highway bridge reference mark were used as benchmarks.

Bulk Sampling and Permeability

Data obtained from bulk samples were entered into a spreadsheet as the weight retained in each sieve class and converted to the cumulative percentage (by weight) finer than the corresponding sieve size. Surface particle size distribution counts (performed before bulk samples were excavated) were entered into spreadsheets as the cumulative percent finer by number (described previously). Sieve analyzed particle size distributions were computed for the three mainstem sites (Figure 21). Surface layer particle size distributions are usually coarser than the sub-surface component in natural gravel-bedded rivers. The SFTFG surface layer was not shaker-sieve analyzed but was hand processed down to >16 mm in the field. Less than 6% of this sample was < 16 mm. SFTFG surface and sub-surface distributions reveal a lower

percentage of fines than the downstream sites. All permeability data for each site was entered into a site spreadsheet file. The permeability worksheet (adapted from McBain and Trush, 2000) takes measurements entered as elapsed time and cm of water inflow, and converts them to inflow rate (ml/s), raw permeability (cm/hr) from a curve generated by Terhune (1958) and Barnard and McBain (1994), final permeability (cm/hr) adjusted by a water temperature factor (Terhune 1958), mean permeability for each sample location, and mean permeability for the entire site. Mean permeabilities computed for each bulk sampling site showed SFTEC (the downstream-most site) to be the highest at 4096 cm/hr (Table 12). The only sampling site available at SFTFG was at a ford and compaction, due to vehicle traffic, may have affected measured permeability.

5.4 WATER TEMPERATURE MONITORING

USFS maintained 33 water temperature sites in WY2002. Table 13 provides a summary of those data, including site location name and map reference number (Figure 10), maximum daily average, maximum temperature, and 7-day running maximum average temperature. Sites are subdivided (by color) in Table 13 and Figure 10 into those sites with 7-day maximum averages greater than 68.4°F (20° C) (in red) and those less than 68.4°F (blue). In general, sites along the mainstem of the South Fork Trinity and along the mainstem of Hayfork Creek exceeded this threshold, and often by a significant amount. 7-day maximum averages for mainstem SF Trinity sites ranged from 66.8 (above Powell) to 78.2 (below Slide), with most sites in the mid to upper 70s. 7-day maximum averages for mainstem Hayfork Creek sites ranged from 77.8 (at Arnold Ranch) to 83.4 (at Hyampom). Hayfork Creek temperatures were the highest in the basin. Many of the smaller tributaries had 7-day maximum averages below or well below the threshold, including Big Creek, Butter Creek, East Fork Hayfork Creek, Eltapom Creek, Powell Creek, and Silver Creek.

5.5 GIS DATA ANALYSIS

5.5.1 Ownership

Detailed ownership maps for the watershed were obtained from a variety of sources including Trinity County and the USFS in a GIS-based format. The majority of the basin is under some form of public ownership, including the Shasta-Trinity National Forest, Six Rivers National Forest, Bureau of Land Management, and various state and county entities.

Figure 22 shows overall ownership patterns in the study area, while Table 14 quantifies the distribution both for the entire watershed and on a study watershed level. In the basin, 82.2% of the area is managed by the U.S. Forest Service mostly in Shasta-Trinity NF, with a smaller amount in Six Rivers NF. A significant amount of the private ownership in the watershed is owned by industrial timberland (Sierra-Pacific Industries, Simpson Timber Company, and Timber Products Company).

Six of the study watersheds are entirely privately owned, while a seventh (Gardner Gulch) is 96.4% privately held. No study watersheds are entirely publicly owned, but 11 of them are over 90% publicly owned.

5.5.2 Slope Analysis

A slope analysis of the watershed was conducted using 10-meter DEM GIS data provided by the U.S. Forest Service. Figure 23 graphically presents the results of this analysis by color-coded slope class. Table 15 summarizes the areas of the entire watershed and the study watersheds by slope class in terms of both acres and percent watershed area. Surprisingly, slopes along South Fork Mountain are mostly in the 20-30% range. Some of the steepest slopes are not in study watersheds, which generally reflect their remote locations with poor access. The steepest study watersheds are Big Canyon Creek, Gardner Gulch, and Shock Creek, all with over 60% of their area with slopes greater than 50%. Overall, about 27% of the watershed has slopes steeper than 50%.

5.5.3 Geology

North Coastal California contains two parallel geologic provinces that differ in age, lithology, structure, and metamorphism: the Coast Range Province and the inland Klamath Mountains Province. The Coast Range Province, containing the well-known Franciscan Assemblage that is composed of unstable sedimentary and volcanic rocks, occupies a small area in southern and northwestern portions of the study area. East of the Coast Ranges are the older Klamath Mountains, underlain by metamorphic and plutonic rocks. The two provinces are separated by the South Fork Mountain Schist, a formation found to be quite unstable after disturbance (Raines 1998).

Figure 24 shows the distribution of geologic terranes in the watershed, while Table 16 summarizes the areas of the entire watershed and the study watersheds by geologic terrane in terms of both acres and percent watershed area. Overall, only 3.4% of the watershed consists of alluvial deposits, reflecting the rugged nature of the basin. About 66% of the watershed is underlain by the Hayfork Terrane, the Rattlesnake Creek Terrane, or granitics, while about 30% is underlain by the more unstable Galice Formation, the South Fork Mountain Schist, and the Franciscan Formation. The division between study watersheds located in predominately stable or unstable geologic settings is evident: Madden, Grouse, Kerlin, Pelletreau, and the SF Trinity above Forest Glen all have the majority of their areas underlain by these potentially highly unstable geologic formations.

5.5.4 Fire History

A fire history of the watershed was developed by combining two GIS coverages, a polygon coverage of larger fires, and a point coverage of smaller fires. These two coverages were merged and data on burned acres by study watershed by decade were obtained. Because of the combination of the two types of data, a figure graphically depicting the fire areas could not be prepared, however, the fire areas by decade and by study watershed in terms of acres and percent are provided in Table 17. Relatively small percentages of the watershed (0-5%) have burned in all decades except the 1980s. 67% of all acres burned by fires in the 1910-2000 period occurred in the 1980s, when over 68,000 acres burned. Significant percentages of certain study watersheds (Butter Creek, Grassy Flats Creek, and Olsen Creek) were burned in this decade. A large percentage of Carr Creek (66%) burned in the 1990s. Otherwise, most study watersheds have relatively little fire history in the past almost 100 years.

5.5.5 Landslides

Landslides mapped during the sediment source analysis for the SF Trinity River are shown in Figure 25 as a point coverage. Since these data come from different sources, not all of which have volumetric data for slide delivery, there was no means of actually computing volumes of landslide delivery by study watershed. The figure does readily depict that most landslides in the watershed are clearly related to the more unstable geologic formations along the western edge of the watershed. Virtually all of the landslides have occurred along the mainstem and west side tributaries, except in the lower watershed, where some landslides have occurred to the east of the mainstem in the Rattlesnake Creek terrane. Very low rates of landsliding are found areas underlain by the more stable geologic formations, such as the Hayfork Creek watershed.

5.5.6 Harvest Areas

Timber harvest has historically been by far the single largest land use activity in the SF Trinity River watershed. GIS-based plantation coverages were obtained from the USFS and harvest areas on private lands were determined by mapping from the 1994 orthophoto quads.

Table 18 and Figure 26 provide the extent of timber harvest in the watershed from about 1970 to 1995. Harvest areas for this period are also presented by study watershed in Table 1. The data indicate that as a whole, about 15% of the watershed has been harvested in the past 30 years. Since there was no way to differentiate the private harvest areas by time period, no attempt was made to evaluate harvest history by decade.

With the exception of several watersheds in Summit Creek watershed (Carr Creek, Gardner Gulch, Shock Creek) and Kerlin Creek, most of the study watersheds had relatively modest amounts of timber harvest (<25%) in the 1970-1995 period. In part, this is the result of many harvest areas not being included in the selected study areas, such as along the lower SF Trinity, or along parts of South Fork Mountain.

5.5.7 Roads

Road data were developed from various sources and compiled into the project GIS. USFS provided much of the base data, which had originally been obtained from the USGS topographic maps. USGS cartographic feature files matching the standard 7.5-minute quad were corrected by USFS to the USGS Digital Orthophoto Quads (DOQs). Newer roads, primarily on private lands, found on the 1994 DOQs were also digitized in order to complete the coverage.

According to the GIS road coverage developed in this study, there are currently 3,035 miles of roads in the SF Trinity Watershed, which translates to a basin-wide road density of 3.26 mi/mi² (Figure 27). Table 19 shows the existing road network distributed by road surfacing type by study watershed. The highest road density in the study watersheds is Kerlin Creek with a density of 5.65 mi/mi², followed by Gardner Gulch at 5.59 mi/mi², WF Rattlesnake Creek (5.33 mi/mi²), and the SF Rattlesnake Creek (5.12 mi/mi²). Notably lower road densities were found in Bear and Little Creeks, in portions of the Barker Creek watershed, and in Madden Creek (< 2.5 mi/mi²).

Surface types were assigned according to data included with the original coverages from USFS and RCD, and all segments added from the DOQs were assumed to be native because of their locations.

6.1 ASSESSMENT OF WY2002 AND 2003 IN HISTORICAL FRAMEWORK

Given the relatively short timeframe of this study, it is important to assess the significance of the water years studied (2002 and 2003) in terms of historical record (i.e. were these wet or dry years?), as this has an important bearing on the interpretation of the sediment yields. There are several means to assess the relative magnitude of these two winters in comparison to long-term historical records of storm intensity, duration, and frequency in order to develop a mechanism for translating data from WY 2001 into average yields (for example a 10-20 year period). Two approaches were used to accomplish this: (1) by comparing annual precipitation totals, and by (2) comparison to flood frequency values for two gages with longer-term flow records in the area (USGS SF Trinity below Hyampom, 1965-present, and USGS Hayfork Creek near Hyampom, 1954-1974).

6.1.1 Precipitation

Precipitation in the SF Trinity Watershed, as is typical of California, is highly seasonal, with 90 percent falling between October and April. Rainfall runoff dominates the hydrologic budget, although depending on location in the watershed and the water year type, snowmelt runoff can be significant. There are few long-term annual precipitation records in the watershed, and instead records from Weaverville were used.

The mean annual precipitation at Weaverville for the 1906-2001 period (96-year record, missing 1981-1983) is 36.29 inches. For Weaverville, the wettest year contained in this record is 1974, when precipitation totals reached 63.58 inches, only slightly wetter than 1998, the next highest, when 63.27 inches were recorded. The driest year at Weaverville was 1977, when only 12.57 inches of precipitation were recorded. For WY2002, annual precipitation in Weaverville was 26.3 inches, considerably below the long-term average. For WY2003, annual precipitation to date is over 36 inches, indicating that this year will be somewhat wetter than normal. However, annual precipitation is only a crude indicator of the geomorphic significance of a given year, as a significant storm may occur in an otherwise dry year.

6.1.2 Flood Frequency

Flood frequency analysis is a method used to predict the magnitude of a flood that would be expected to occur, on average, in a given number of years (recurrence interval) or to have a specific probability of occurrence in any one year (1% chance event, for example). Typically, the observed annual maximum peak discharges are fitted to the distribution using a generalized or station skew coefficient, although numerous other distributions may also be used. When long records are available, the station skew is generally used exclusively. DWR (1991) and GMA (1998) and included flood frequency of the USGS gage records using the Log-Pearson Type III distribution for the gages' respective periods of record. For Hayfork Creek near Hyampom, the Q_2 event (flood event that would occur on average once every 2 years) was 12,000 cfs and Q_5 was 20,000 cfs. Although the GMA gage on Hayfork Creek near Hyampom was not installed until after the annual maximum peak flow in WY2002, it is estimated that the return interval of the peak discharge was less than a two year event. In WY 2003, the computed peak discharge of 15,600 cfs has a recurrence interval of 3-4 year flow. Data for the USGS gage below Hyampom were not yet available at the time of this report.

6.2 WATERSHED LEVEL RELATIONSHIPS

Figure 16 shows the combined relationship of suspended sediment load versus discharge for ten datalogger sites. The combined relationship has an R^2 value of 0.73, although there is almost 3 orders of magnitude difference between extreme data points in portions of the relationship. Overall, little can be

learned from watershed level relationships. Figure 17 segregates these same data points into individual station curves, revealing improved relationships, and illustrating real differences between sites.

6.3 INDIVIDUAL SITE RELATIONSHIPS

One of the best ways to compare individual sites with divergent watershed areas is by normalizing discharge by watershed area. In Figure 17, suspended sediment load versus unit discharge (cfs/mi²) is presented for the ten datalogger stations.

Preliminary analysis of these data yields a number of conclusions:

- Tule Creek has substantially lower sediment yields than the other sites. Tule Creek drains a watershed with stable geology, has moderate road density (3.77 mi/mi²), and 15% of the watershed has been harvested in the last 25 years. Tule Creek has relatively mild slopes and is 96% publicly owned, thus the harvest probably occurred at least 10 years ago. It would appear that the combination of moderate slopes and stable geology and lack of recent harvest, results in low suspended sediment transport rates.
- Hayfork Creek near Hayfork has somewhat greater transport rates that Hayfork Creek near Hyampom. This implies that the watershed between these sites has much lower sediment yields. Hyampom Road traverses Hayfork Creek's lower gorge by staying high on the ridge, reducing the likelihood of hydrologic connectivity between road and stream system. Almost all of this watershed area is federally owned, and has relatively low levels of disturbance (harvest, roads, or development).
- Summit Creek and SF Trinity at Forest Glen have very similar sediment transport rates per unit discharge. This occurs despite extreme differences in geology and land use. At present, there is no apparent explanation for this.
- Barker Creek at Stokely Ranch and Hayfork Creek near Hayfork have similar transport rates and are the highest of the six sites computed to date. The Barker Creek watershed is underlain by stable geology (Hayfork Terrane), has moderate slopes (25.6% of the watershed has 50% slopes or steeper), a moderate road density (3.25), and low harvest rates (8.9%). The only apparent explanation for these high transport rates lies in the road network and the effects of land use in the privately held portions. The sites contributing to Hayfork Creek near Hayfork have much lower rates of suspended sediment transport, implying either (1) most of the sediment load is delivered via the mainstem of Hayfork Creek, or (2) some stations (like Salt Creek) need more high flow measurements to accurately predict the sediment loads. Barker Creek is examined in greater detail in the next section.
- In WY 2003, Grouse Creek produced more suspended sediment than any other station (64,000 tons), and with a basin area of only 53.2 miles, also produced the highest SSLPA, at 1,200 tons per square mile (Table 9). Due to its proximity to the coast and local orographic effects, Grouse Creek encounters high flows at times when the rest of the basin often shows limited response. Due to the frequency of such flows, its unstable geology, and road density in the inner gorge, Grouse Creek transports sediment at very low flows and at very high rates at increasing flow (Appendix C-26). However, sediment loads computed for WY2003 are far below the long-term rate developed by Raines and Kelsey (1991) which averaged 4,990 tons/mi/yr in the 1960-1990 period. Since WY2003 was a wetter than average year with peak flows in the 3-4 year range, it might be expected that sediment loads would be greater than the long-term average. This could suggest that restoration activities and improved road maintenance and harvest practices have been successful in reducing chronic sediment yields observed in the 1960-1990 period.
- Eltapom Creek was included to describe a less-disturbed watershed, but until more samples and

high flow measurements are performed, load predictions will remain uncertain.

- Big Creek at Highway 3 and Barker Creek at Stokely Ranch have nearly identical SSLPA curves. They flow nearly parallel to one another, have similar percent areas harvested and drain the same geologic types, but Barker has higher road densities and a greater percentage lying in private ownership. High flow measurements at each site may help define relationships more clearly. Otherwise, no explanation for the similarity is currently apparent.
- Differences between the highest and lowest sediment transport rates per unit discharge of these ten sites are greater than an order of magnitude for study watersheds in similar geologic terranes. Differences must be related to land use.

6.4 DETAILED STUDY WATERSHED SITE RELATIONSHIPS

Two watersheds, Barker Creek and Rattlesnake Creek, were selected for more detailed evaluation of sediment loading, and to identify possible imbalances in sediment production. 6 or more manual stations were established in Barker Creek and Rattlesnake Creek watersheds to compare sediment transport rates and yields from a variety of smaller sub-watershed areas. Within each of these watersheds, most key tributary and accessible sites were monitored. A third study watershed (Cedar Gulch) provided insight into the effects of a single land use (riparian grazing) on turbidity in that channel.

6.4.1 Barker Creek

Setting

Barker Creek is a 10.2 square mile watershed flowing north to south into Hayfork Creek approximately four miles upstream of the town of Hayfork. The headwaters originate near 5,800 foot Barker Mountain while the confluence with Hayfork Creek lies at 2,460 feet (Figure 28). Barker Creek drains USFS and private timberland lands in its upper reaches and mostly private residential properties in its lower reaches. The mainstem of Barker Creek supports runs of anadromous salmonids and is essentially a perennial stream, though some reaches flow sub-surface during the dry season. The smaller tributaries flow intermittently and some flow only during storm events. Following heavy winters, the mainstem shows a pronounced snowmelt hydrograph while some of the downstream tributaries may be dry. Consequently, discharge relationships between the mainstem and its tributaries vary with hydrograph position, type of storm, location/aspect and drainage area.

Habitat attributes, the wide spectrum of land-use management practices, and the apparent high sediment load in Barker Creek, dictate examining this watershed in a detailed manner to describe the hydrology of its sub-basins, and ascertain regions of higher sediment production.

Gaging

Gage locations were chosen based on access and with respect to differing patterns of land use. A continuous recording datalogger was installed on the mainstem at the Stokely Ranch (BCSR) in November 2001, and served as the primary gage for continuous records in the basin. Unfortunately, this datalogger failed twice during Water Year 2002. For both periods, a synthetic discharge record was developed from the gage at Summit Creek at Wildwood Road. Several methods (including basin area relationships and rise/fall patterns) were compared and the most accurate (based on actual stage observations during the predicted period) proved to be a regression equation developed for a period of rise/fall during a large storm. The hydrograph was further adjusted to reflect actual stage values recorded from crest gages (Figure 14). A new datalogger functioned well throughout WY 2003 (Figure 29). Another datalogger installation site was attempted near the Hayfork Creek confluence (at the Highway 3 crossing), but ultimately failed due to hydraulic control issues and lack of access to an adjacent, more appropriate gaging site. A stage reference and crest gage were established instead and Barker Creek at

Highway 3 (BCH3) was operated as a manual station, with the assumption that continuous flow records could be generated from the BCSR gage less than a mile upstream.

Between BCSR and BCH3, a small second order tributary enters from the east. This tributary is deeply incised into alluvial soils and appears to have lost access to its floodplain. The segment downstream of Barker Valley Road is even more deeply incised below the shotgun outlet of twin 36 inch CMPs. Above Barker Valley Road, we installed a crest gage (BTBV) and another below (BTSR), to compare stream discharge and sediment production above and below the road crossing. The drainage areas for the two gages are 0.57 and 0.63 square miles respectively.

Little Barker Creek at Barker Creek Road (LBBC) drains 2.07 miles of mostly USFS land. This manual station is located approximately 300 feet downstream of Barker Creek Road. Upper Barker Creek at USFS Road 32N03 (UB03) drains 5.36 square miles and is located on the mainstem of Barker Creek.

Streamflow

Stage-discharge relations were developed for most stations based on actual discharge measurements as described previously, however, three of the sites presented unique challenges related to their respective hydraulic controls. Discharge measurements were made for BTBV up to 11.9 cfs (Table 20), but due to the extremely flashy character of this stream, it was impossible to get high flow measurements during storms, as sampling priorities dictated efforts elsewhere. A slope-area measurement was attempted following a small peak on April 29, 2003. A plot of the water surface profile shows the energy gradient (water surface slope) to be greatly reduced from a back-watering effect of the culvert/road crossing, precluding the assumptions of the slope-area measurement (Figure 30). This back-watering effect could not be detected visually during storm peaks, but greatly affects the stage-discharge rating. Since the exact flow at which the gage is back-watered is unknown, following standard USGS protocols, the low water rating was extended to twice the maximum observed discharge value (to 23.8 cfs), but sediment samples were taken at much higher flows. Assuming the gage becomes back-watered somewhere above 23.8 cfs and since the rate of change in stage vs. discharge decreases markedly in a back-watered condition, a synthetic rating was developed (to prevent over-estimating BTBV discharge) by comparing stage heights at known BTBV discharges with known discharges at BCSR. Using measured discharges at BTBV (and one rated observation of 22 cfs), comparisons with BCSR discharges yielded an average of 17% and this value was used to develop the synthetic BTBV rating for flows above 22 cfs (Figure 31).

The BTSR site, just downstream of BTBV, lies in an extremely brushy channel, prone to debris and fine sediment accumulation during peak flows and offers no reliable stage reference. Sediment samples were usually taken within 10 minutes of a sample taken at BTBV. No rating curve was developed for BTSR and discharge values for sediment samples were taken as the percent increase in basin area from BTBV (9%).

Barker Creek at Highway 3 is a crest gage located approximately 10 feet upstream of the concrete box culvert passing under Highway 3. Stage reference elevations are surveyed to the crest gage and to marks on the culvert wing walls. The bottom of this culvert is roughened by baffles and a fish ladder connects Barker Creek to Hayfork Creek. Wading measurements were performed up to 64 cfs. The only appropriate flow measurement section is at the culvert entrance, which becomes extremely dangerous to wade during high flows and the site is inappropriate for bridge techniques (Figure 32). During the 64 cfs measurement, BCH3 was 23% higher than BCSR during a steady decline. In periods of low flow, accretion between BCSR and BCH3 can be zero (when BTBV and BTSR are dry), and during peaks may be much higher than the observed 23%. In order to accommodate the variability in the relationship between BCSR and BCH3, the measured rating curve at BCH3 was used up to 128 cfs (twice the highest measured discharge) and above this, a synthetic rating was developed using an assumed average increase

of 27% of the BCSR discharge during peak flows (Figure 33). The 27% increase was derived from: (1) the 17% average from BTBV plus an additional 9% accretion from BTSR (based on percent basin area) plus another 1 % from percent basin area between BTSR and BCH3, and (2) observations of simultaneous stage at BTBV and BCSR suggest a potential range of peak flow accretion from 17% to 38% (from BCSR to BCH3) and 27% is the approximate mid-point of this range. The BCH3 discharge rating could be improved by surveying and rating the concrete box-culvert, and comparing rated stage values with observations from BCSR.

Discharge Hydrographs

The discharge hydrograph for BCSR served as the primary component for developing hydrographs for the rest of the stations in the Barker Creek watershed. Synthetic hydrographs were generated for all stations based on the same relationships (if used) to develop rating curves. Streamflow for BCSR was measured up to 101 cfs to develop the discharge rating and the hydrograph predicts flows up to 311 cfs. Since this exceeds the standard of projecting beyond twice the highest measured discharge, peak flow values may be in error. In the absence of a better predictive approach, this method allows a general comparison of Barker Creek sub-basin hydrology. In all Barker comparisons, the most conservative choices were made to prevent over-predicting discharge. All synthetic hydrographs were checked against observed stage heights and measured discharge relationships were used over rated discharges when possible. Qualitative observations during sediment sampling suggest that the downstream sites (BTBV, BTSR and BCH3) may peak higher than our estimates indicate.

Since BCH3 shows a greater increase from BCSR during storms than during periods of low flow (when BTBV and BTSR are dry or very low), high flows were increased by 23% of BCSR and low flows were increased by 11%. The lower value represents the lowest observed rate of accretion (for a measured discharge taken when BTBV is flowing), and the higher value represents the observed accretion during a steady decline from a peak flow at BCH3. This approach likely over estimates low flows at BCH3 (such as when BTBV is dry) and under-estimates some peaks (because BTBV is capable of producing much more than 23% of BCSR during some events). A BCSR discharge value 66 cfs was chosen as the cut-off between high and low flow relationships, because at 66 cfs, BTBV was 17% of BCSR, the approximate mid-point of high and low flow relationships. Stage observations agree with all synthetic hydrographs (Figure 34).

A synthetic hydrograph was developed similarly for BTBV using 11% and 21% of BCSR respectively for low and high flow percentages. The 11% represents the relationship when a discharge of 3.02 cfs was measured at BTBV, while the higher value represents the percentage observed for the highest BTBV stage observation within the measured rating (23.8 cfs) (Figure 35). BTSR was generated with the increase of BTBV by 9%, as detailed in the rating description.

BCSR and UB03 each occupy the mainstem of Barker Creek and as a consequence have similar responses to most storms. Discharge measurements made within 1 hour of one another during a period of steady decline from a snowmelt-influenced peak (January 14, 2003) showed UB03 to be 58% of the flow at BCSR. The drainage area ratio for these two sites is also 58%. For three peaks in January and February of 2002, however the discharge ratio proved to be 40%. These percentages were averaged for the entire record and UB03 was generated as 49% of BCSR.

The January 2002 peak crest gage stage at LBBC was rated at 52 cfs, 22% of the rated peak at BCSR. Since the drainage area ratio is 21%, the value of 22% was accepted and the entire hydrograph was generated with this value.

Suspended Sediment

Suspended sediment loads versus discharge ratings were computed for all six Barker stations (Appendix C). The two upstream-most sites (UB03 and LBBC) showed great variability in the relationship between SSL and discharge and were examined for hysteresis based on:

- 1. field observations during storms
- 2. apparent strata in the data set
- 3. known patterns of suspended sediment production.

Separate SSL ratings were developed and applied accordingly to periods of rise/fall on the synthetic 15 minute discharge hydrographs (Appendix C-5, 6). Suspended sediment rating equations were applied to the other four 15-minute discharge hydrographs to generate sediment transport totals for WY 2002 and WY 2003 (Table 21).

To facilitate comparisons between rates of suspended sediment production, suspended sediment loads per unit discharge (normalized by drainage area) were computed for all six sites (Figure 36). Total loads by site (averaged for WY 2002 and 2003), were plotted against basin area to compare sub-basin sediment loads (Figure 37). Barker Tributary at Stokely Ranch produced more suspended sediment per square mile than any station except Grouse Creek (Table 9).

Discussion

Most of the sediment production in the Barker Creek basin occurs in the downstream portion of the watershed. Sediment production will be discussed here in terms of an evolution in rates and sediment totals from upstream to downstream, using BCSR, the station with the best data, as the primary comparator. UB03 has a drainage area (5.36 square miles) 58% as large as BCSR, but its sediment load is only 9-11% of the sediment load at BCSR (Table 21). LBBC represents another 22% of BCSR's drainage area but contributes only 2-3% of the sediment load observed at BCSR. Apparently, at least 86% of BCSR's sediment load is delivered in the 1.83 square miles downstream of UB03 and LBBC.

Another major sediment source for Barker Creek contributes between BCSR and BCH3, where the sediment load nearly doubled, from 1324 tons to 2404 tons, in WY 2003 (Table 21). BTBV contributes 285 tons from the reach above Barker Creek Road, which increases to 618 tons a few hundred yards downstream at BTSR. Subtracting the load at BCSR from BCH3 (1080 tons) suggests another 462 tons (1080-618) is delivered below BCSR and BTSR.

The deeply incised channel below Barker Creek Road is essentially a gully formed in highly erodible material. For a corresponding increase in discharge, water depth in such channels achieves greater depth than in streams exhibiting active channel-bankfull-floodplain morphology, greatly increasing potential for scour and sediment entrainment. The normalized rates in Figure 36 show that while BTSR sediment production greatly exceeds the other streams up to about 11 cfs/square mile, beyond this point, both BCSR and BCH3 produce more sediment per unit discharge increase than BTBV. Incised streams like BTBV and BTSR with little tributary input and no access to the floodplain may achieve some maximum rate of entrainment of bed and bank material. The Barker Valley Road drainage system may contribute discharge/sediment up to some maximum rate in similar fashion. The fact that the normalized SSLPA curve for BTBV falls well to the right of the others, while its total load/basin area is so high, is an artifact of the normalized discharge on the X axis: at 20 cfs/square mile, BCH3 is producing sediment near its observed maximum (at 200 cfs), while BTBV is producing near the observed mid-range (at 11 cfs). Because BTBV encounters its higher transport rates more often than the larger streams, its curve sits to the right, but its total annual tons/square mile is exceeded only by BTSR.

Restoration or sediment control priorities for the Barker Creek watershed could be determined as follows:

- 1) If Barker Creek mainstem aquatic habitat is the priority, then sediment sources below UB03 and LBBC should be assessed: Barker Tributary at Stokely Ranch affects only the extreme downstream segment of the mainstem.
- 2) If chronic sediment sources affecting the entire watershed are the priority, then a geomorphic investigation into the processes driving the channel morphology and rates of sediment production from BTSR should be conducted. Barker Tributary is a very small watershed producing an extremely high sediment load: road improvement or instream restoration efforts applied to relatively small geographic area could result in the greatest reduction in suspended sediment per unit effort.

6.4.2 Rattlesnake Creek

Rattlesnake Creek flows alongside State Highway 36 for most of its length. Inner-gorge road construction along the lower five miles of Rattlesnake Creek results in highly erodible cut/fill slopes and adds miles of ditch length to the stream network. Two manual stations are located in relatively pristine (un-roaded) tributary basins (WFSFR and SFR57). UR73 and UR36 describe the mainstem of Rattlesnake Creek. Post Creek (PCH36) runs adjacent to USFS 30N54 (and several other roads) for much of its length. NFR14 and LRGS are less heavily roaded than the mainstem stations, but little useful data were collected at these two stations due to access issues and site appropriateness.

The USFS datalogger on Rattlesnake Creek (RC29) was intended to tie together the seven manual stations upstream. Hydrographs from RC29 would facilitate development of synthetic hydrographs for the manual stations and subsequent load computations for each sub-reach. The Rattlesnake gage height record could not be used however: an accurate discharge rating was not developed, the stage reference shifted, and the gage itself was destroyed by the WY2003 peak flow. SSLPA curves were computed for the Rattlesnake Creek manual stations for which adequate data were collected and for which accurate rating curves were developed (Figure 38).

The upstream-most station (UR73) clearly stands out as having the highest rate of increase in suspended sediment production. The rate decreases downstream (at UR36), presumably due to dilution by WFSFR and SFR57. Post Creek shows the lowest rate of increase in sediment production (exponent = 1.12) relative to the other sites. However, the rating curve at PCH36 was only developed up to 108 cfs (gage height = 2.35 ft), and samples were taken up to a gage height of 5.3 feet. Sediment samples taken at gage heights up to 3.82 feet were included in the analysis. Qualitative observations during sampling (Post Creek becomes turbid very quickly during storms) suggest one of two possible scenarios:

- 1. Post Creek is somehow supply-limited above a certain discharge threshold, producing relatively high sediment loads at lower flows but not increasing as rapidly as the mainstem stations. This could be related to pulses of sediment from road surfaces and other development in the watershed.
- 2. The discharge rating for PCH36 is inadequate for accurate predictions above twice the highest measured discharge (216 cfs).

The latter scenario seems most likely. High flow measurements on Post Creek are required to define the upper end of the rating curve, which would allow a more useful interpretation of the PCH36 SSC dataset. *6.4.3 Cedar Gulch*

Cedar Gulch is a small ephemeral tributary to Hayfork Creek about 1 mile west of the town of Hayfork. These sampling sites were included in the study due to the fortuitous presence of a volunteer observer who lived in the upper part of the watershed. His personal observations indicated that land use activities along the lower reaches of the stream appeared to contribute a substantial amount of sediment. The area downstream of New Country Lane is heavily grazed by cattle and horses and no riparian fencing is present, providing the livestock complete access to the stream channel on a year round basis. Visual observations indicated heavily trampled banks and very little riparian vegetation present along the channel. Due to the small size of the channel and the relatively low priority of these sites, no discharge data were collected at either of the sites. The study consisted of upstream and downstream sites, measured in a synoptic fashion, and samples collected were analyzed for turbidity and suspended sediment concentration. Figure 39 presents the comparison of upstream and downstream sites on the dates that both were measured within a few minutes of each other. In virtually all cases, turbidity values were higher at the downstream site, sometimes by 30%, but often by 100% or more. The largest differences were observed during high flow periods, particularly in December 2002, when turbidity increases of 400-600% were observed. The highest turbidity values observed at the upstream site was 28 NTU, while the highest value at the downstream site, below the grazing disturbance area, was 140 NTU. Suspended sediment concentrations were even more greatly impacted by this land use with the increase in SSC between the two sites ranging from 146-1500%. Clearly, localized land use activities can have a substantial effect of sediment yields.

6.5 ANALYSIS OF SEDIMENT LOAD VALUES BY GEOLOGIC TERRANE

Figure 24 shows the study sites overlain on a simplified geologic map of the watershed. The WY2002-2003 data were stratified by geology to evaluate possible differences between sediment generation and transport rates in the various geologic terranes. As depicted in Figure 1, seven of the ten datalogger sites computed lie in the Hayfork Creek watershed and generally have similar geology. Given the scatter observed in these analyses, it is apparent that geology by itself does not explain much of the variability between watersheds in terms of observed sediment loads or turbidity. Grouse Creek, draining Sedimentary Alluvium and Franciscan regions, and with its high percentage of landslides (Figure 25), may represent an exception. The extent of management activities appears to play a more significant role than geology in determining sediment yields.

6.6 RELATIONSHIP TO TMDL DATA

Raines (1998) developed management and non-management sediment yields as part of the sediment source analysis for the South Fork Trinity River. Total rates (management and non-management rates combined) were 317, 282, and 182 tons/mi²/yr for the 1975-1990 period for the Lower South Fork, Upper South Fork, and Hayfork sub-areas, respectively. This is the most recent and comparable period to the rates computed in this study. For the Hayfork Creek near Hayfork site, WY2003 suspended sediment yield was computed at 158 tons/mi². Although this is only the suspended sediment portion of total load, the bedload component is unlikely to be more than 10% of the suspended load. Thus, for WY2003 the estimated total yield of Hayfork Creek is approximately 173 tons/mi². Given that the peak discharge in WY2003 was apparently a 3-4 year event, this implies that the average sediment yield would likely be smaller than WY2003. Thus, the yield estimates for Hayfork Creek from the TMDL would appear to be somewhat higher than those measured. However, these values are still relatively similar and well within the range of accuracy of such computations. Without more extensive data, any such conclusions must be considered speculative.

6.7 COMPARISONS TO HISTORIC DATA

Comparisons to historic data are only possible for certain data types and in certain areas only. Most of the older historic data are found only in the vicinity of gaging stations, which were only on the mainstem (USGS Forest Glen, near Hyampom, below Hyampom, and near Salyer gages) or the two on Hayfork

Creek (USGS near Hayfork and near Hyampom gages). Recent comparisons to historic mainstem data and selected tributaries (Pelletreau Creek) were provided by GMA (1998). Follow-up surveys at several of these sites were conducted by USFS (2001). In general, mainstem data were interpreted to show continued progress towards overall channel recovery from the devastating effects of the December 1964 flood, though the period of recovery is likely to be on the order of decades to centuries (GMA 1998, USFS 2001). No data on Hayfork Creek were developed for either of these previous geomorphic investigations. No additional data at these sites were collected as part of this study (except SF Trinity at Forest Glen, although the GMA surveys are not directly comparable to USGS data from the 1960s due to apparently differing sites), as these sites are part of USFS monitoring efforts.

More recent historic geomorphic data are available from USFS surveys in late 1980s and in the 1990s at Butter Creek, Pelletreau Creek, Grouse Creek, and, when possible, these sites were re-occupied in this study. Unfortunately, none of the USFS cross section pins on Grouse Creek could be relocated, and without an equivalent datum, no comparison of the long profile could be made.

Two cross sections were reoccupied on Butter Creek that were originally surveyed by USFS in 1989. USFS Cross Section #4 is equivalent to GMA cross section number 5. Only small differences are found between the surveys 13 years apart. There has been a net scour at this cross, although the magnitude is small (less than 1-foot of change).

Five cross sections were re-occupied at Pelletreau Creek and for most of these cross sections data were available from 1989 and 1997. Cross section #1 changed substantially between 1989 and 1997, but remained stable from 1997 to 2002. Cross section #2 changed and aggraded substantially between 1989 and 1997 and then by 2002 it had incised back to the 1989 thalweg elevation and most of the 1997 aggradation material was removed. Cross Section #3 experienced net degradation between 1989 and 2002 (no 1997 data were available). Cross section #4 showed channel aggradation but net stored sediment removal between 1989 and 1997, then substantial scour and further removal of stored sediment between 1997 and 2002. Cross section #5 showed substantial channel migration and bank erosion, but little change in thalweg elevation between 1989 and 2002 (no 1997 data were available). It is apparent that this reach of Pelletreau Creek is unstable and changes in large storm events due to influxes of sediment (1997 event), but that overall, stored sediment is being removed.

The cableway cross section at the former USGS Hayfork Creek at Hyampom gage was also re-surveyed, but the historic USGS cableway measurements from the 1960s to mid seventies were not available at the time of report preparation.

Due to substantially differing methods (much larger volumes and subdivision of surface and sub-surface populations, data obtained from bulk sampling in this study are not likely to be comparable to earlier DWR or CDFG substrate datasets.

7.0 CONCLUSIONS AND RECOMMENDATIONS

Although not all of the data collected in this study have been computed as of this date, the following conclusions have been developed and are presented here:

- Significant differences between sediment transport rates have been observed at the ten datalogger sites.
- The relative stability of the various geologic terranes appears to have little relationship to sediment yield for most of the studied sites in WY2002 and 2003.
- The highest sediment transport rates among datalogger sites were found at the Hayfork Creek near Hayfork site at 211 tons/mi² and at Grouse Creek at 1,200 tons/mi². As mentioned previously, Grouse Creek appears to be in its own unique strata, which is likely due to a combination of management and geologic stability factors. Unit sediment yield varied by a factor of 6 between the other 9 sites (excluding Eltapom Creek due to an incomplete record).
- Though treated separately, three of the Barker Creek sub-watershed station totals exceeded all datalogger sites except Grouse Creek.
- Sediment yields do not appear to be related to simple metrics of watershed disturbance such as road density or percent watershed harvested.
- A detailed program of streamflow and sediment transport measurement has quantified substantial differences in sediment yield between sites.

The following recommendations are made:

- Although not all sites were computed, review of data collected within sub-watersheds indicates that measurement of streamflow and sediment transport can be an effective technique to identify sub-watershed areas that are producing sediment at higher rates.
- The strength of relationships between turbidity and suspended sediment for individual sites, suggests that measurement of turbidity could define sediment yields at a management level once streamflow rating curves had been developed. Since turbidity is far easier and less expensive to measure than suspended sediment, this may be a more cost effective approach to evaluating relative sediment yields. In addition, technology is now available to monitor turbidity continuously, even at fairly remote sites.
- Developing sediment and streamflow records for the USFS datalogger station on upper Hayfork Creek could provide substantial resolution for understanding sediment loads at Hayfork Creek near Hayfork.
- Improvement to and successful operation of the USFS datalogger station on Lower Rattlesnake Creek would allow development of synthetic streamflow records and subsequent computation of sediment loads for the Rattlesnake Creek sub-watershed stations.
- High flow measurements or slope-area estimates of discharge would greatly increase the accuracy of load estimates at the following stations using existing sediment load ratings: BGCH3, BCH3, BCSR, SCSCG, BTBV, and PCH3.
- The peak flows of WY 2003 justify repeating the geomorphic component of this study.

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SOUTH FORK TRINITY RIVER WATERSHED General Site Descriptions for Sites Administered by Graham Matthews and Associates

GEOGRAPHIC UNIT	SITE #	SITE NAME	AC	CRONYM	Watershed Area (mi ²)	Datalogger installed	Crest Gage Installed	Geomorphic Reach Established
Barker Creek	1	Barker Creek at Hwy 3		BCH3	10.17		ves	
	2	Barker Creek at Stokely Ranch		BCSR	9.26	yes	yes	
F	3	Barker Trib. at Barker Valley Rd.		BTBV	0.57	900	ves	
	4	Little Barker at Barker Cr. Rd.		LBBC	2.07		yes	
F	5	Upper Barker at USFS 32N03		UBO3	5.36		ves	
	6	Barker Trib. at Stokely Ranch	E	BTSR	0.63		yes	
pper Hayfork Creek	7	Big Creek at Hwy 3	В	IGCH3	27.26	yes	yes	
	8	Carr Creek at Hwy 3	(CCH3	5.96		yes	
	9	Duncan Creek at Summit Creek Rd.	D	CSCR	6.47		yes	
	10	Gardner Gulch above Pond		GGAP	1.27		yes	
	11	Shock Creek above Gardner Gulch	-	CAGG	1.53		yes	
	12	Summit Creek at Summit Creek Rd.		SCSCR	2.53		yes	
	13	Summit Creek at Wildwood Rd.		SCWR	28.26	yes	yes	
ower Hayfork Creek	14	Bear Creek above Hayfork Creek		BCHC	7.63	yes	yes	
	15	Hayfork Creek near Hayfork		HCNH	265.10	yes	yes	yes
	16	Little Creek at Hyampom Rd.		LCHR	9.09		yes	
	17	No Name at 9 Mile Bridge.		IN9MB	2.67		yes	
	18	Salt Creek at Salt Cr. Growers		SCSG	53.59	yes	yes	
	19	Tule Creek at Tule Creek Road		CTCR	20.25	yes	yes	
yampom	20	Big Canyon Cr. at Hyampom Rd.		BCHR	1.82		yes	
	21	Butter Creek		UCSFT	36.08	yes	yes	yes
	22	Eltapom Creek above South Fork Trinity		CASFT	19.59	yes	yes	
	23	Grassy Flats at Hyampom Rd.		GCHR	2.16		yes	
_	24	Grouse Creek	-	CASFT	53.18	yes	yes	yes
_	25	Hayfork Creek near Hyampom		HCHY	378.77	yes	yes	yes
	26	Kerlin Creek at Hyampom Rd.		KCHR	3.96	yes	yes	
_	27	Olsen Creek at Olsen Creek Rd.		COCR	6.40		yes	
	28	Pelletreau Creek at Hyampom Rd.		PCHR	11.80	yes	yes	yes
orest Glen	29	South Fork Trinity at Forest Glen		SFTFG	207.58	yes	yes	yes
	30	South Fork Rattlesnake at 29N57		SFR57	1.98		yes	
_	31	Upper Rattlesnake above 29N73		UR73	6.74		yes	
_	32	Upper Rattlesnake above Hwy 36 Water Hol		UR36	14.47		yes	
	33 34	W. Fork of S. Fork Rattlesnake at 29N57 Madden Creek at Route 6		VFSFR MCR6	1.52 22.53		yes	
ower S.F. Trinity	34	Maddell Cleek at Roule 6		VICRO	22.03	yes	yes	
Aainstem Sites: Bulk Sampling		South Fork Trinity at Forest Glen	5	SFTFG	1			
ind Spawning Gravel	-	South Fork Trinity at Hyampom Road		SFTHR				
Permeability	-	South Fork Trinity near Eltapom Creek		SFTEC	1			
,					1			
			т	OTALS				
		Continuous Data Recording (datalogger) Stat	tions	15				
		Manual (crest gage only) Stat		19				
		Geomorphic Monitoring		6				
		Bulk Sampling		3				
				-				

##
							TOTAL #
SUB-UNIT	SITE NAME	ACRONYM	# MEASUREMENTS WY2001	# MEASUREMENTS WY2002	# MEASUREMENTS WY2003	SLOPE AREA MSMTS. WY2002-2003	MEASUREMENTS BY SITE
Summit Creek	Summit Creek Summit Creek Rd	SCSCR	2	1	0		3
Summit Creek	Carr Creek	CCH3	3	1	1		5
	Shock Creek	SCAGG	2	1	0		3
	Gardner Gulch	GGAP	2	1	0		3
	Duncan Creek	DCSCR	3	1	1		5
	Summit Creek Wildwood Rd	SCWR	4	3	1	1	9
					I	•	5
Barker	Upper Barker	UBO3	0	5	1		6
	Little Barker	LBBC	0	3	1		4
	Barker Trib Barker Valley	BTBV	0	3	3		6
	Barker Creek Stokely Ranch	BCSR	0	4	3		7
	Barker Creek Highway 3	BCH3	2	1	3		6
Hayfork Valley	Big Creek	BGCH3	3	3	3		9
,,	Salt Creek	SCSG	0	8	5		13
	Tule Creek	TCTCR	0	5	4	2	11
	Hayfork Creek near Hayfork	HCNH	7	3	3	2	15
		1.0115		<u>^</u>			
Hayfork-Hyampom	Little Creek	LCHR	0	3	1		4
Road	No Name at Nine Mile Bridge	NN9MB	0	2	2		4
	Grassy Flats	GCHR	0	2	1 0		3
	Big Canyon Creek Olsen Creek	BCHR OCOCR	-	3	0		5
	Bear Creek	BCHC	2	6	2		8
	Dear Creek		U	0	2		0
Rattlesnake	Upper Rattlesnake Hwy 36	UR36	0	6	2		8
	Upper Rattlesnake Rd 29N73	UR73	0	5	2		7
	WF SF Rattlesnake	WFSFR	0	4	1		5
	SF Rattlesnake	SFR57	0	4	2		6
	Post Creek	PCH36	0	4	3		7
	NF Rattlesnake	NFR14	0	2	1		3
	Rattlesnake Creek	RC29	0	3	2		5
Forest Glen	Glen Creek	GGGR	0	2	2		4
	SF Trinity Forest Glen	SFTFG	0	7	1	4	12
Hyampom	Butter Creek	BUCSFT	0	7	3		10
nyampon	Pelletreau Creek	PCHR	0	8	2		10
	Kerlin Creek	KCHR	0	5	1		6
	Eltapom Creek	ECASFT	0	7	0		7
	Hayfork Creek at Hyampom	HCHY	0	6	2	1	9
Lower Watershed	Grouse Creek	GCASFT	0	9	5	3	17
	Madden Creek	MCR6	0	4	1		5
TOTAL DISCHARGE	MEASUREMENTS	253					

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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SOUTH FORK TRINITY RIVER WATERSHED Discharge Data Collection Summary for 10 Datalogger Stations WY 2002 and 2003

		w	Y 2002	WY	2003
Station	Total # of Streamflow Measurements	Date	Peak Discharge (cfs)	Date	Peak Discharge (cfs)
BCSR	7	1/2/2002	258	12/28/2002	311
SCWR	9	1/2/2002	897	12/16/2002	1,430
BGCH3	9	1/2/2002	845	12/16/2002	964
HCNH	15	1/2/2002	11,000	12/16/2002	13,500 **
SCSG	13	N/A	N/A	12/16/2002	3020
TCTCR	12	1/2/2002	957	12/28/2002	1,000
HCHY	9	2/20/2002	3,590 *	12/16/2002	15,600 **
SFTFG	12	1/2/2002	7,200 **	12/16/2002	11,600 **
ECASFT	7	1/2/2002	647	12/16/2002	711
GCASFT	18	1/2/2002	1520**	12/28/2002	5800**

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* gage installed after annual peak flow

** peak flow determined by slope-area method: all others by extensions of rating curve

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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TABLE

					G							Restora		23				
			P. 0.	Box 151	16 Weaver	ville, CA	96093-1	516 Pho	ne: (530)	623-5327	Fax (530) 623-5328	3; email: gra	ham@gr	mahydro	logy.com		1
							DISC	HAR	GE S	UMN	IARY	SHE	ET					
		L	OCATION:	Sout	h Fork	Trinit	y Riv	er at I	orest	Glen			WAT	ER Y	EAR:	2002, 2003	}	
easuremen		Date	Made By:	Width	Mean	Area	Mean	Gage	Discharge	Rating		Method	No. of Msmt	Begin	End	Msmt	Recorder	Notes
Number	Momt #			(feet)	Depth (feet)	(ft²)	Velocity (ft/sec)	Height (feet)	(cfs)	Shift Adj.	Percent Diff.		sections	Time (hours)	Time (hours)	Rating	level	
1	2002-01	11/15/2001	S. Pittman	60.3	1.31	79.20	0.53	0.76	42.30		-5%	10/ a dia a	43	900	1130	Good		
2	2002-01		S. Pittman	79.5	2.36	188.00	0.55	1.31	42.50		-5%	Wading Wading	43 39	1030	1122	Good		AA malfunctioned; used pygmy
2	2002-02		Pittman/Pryor	n/a	n/a	n/a	n/a	3.38	1010		-3%	Boat	12 passes		1235	Good		ADP measurement
4	2002-04		S. Pittman	76.0	3. 2	230.00	2.11	2.45	486		-2%	Wading	31	1355	1540	Good		
5	2002-05		S. Pittman	90.0	2.01	181.00	1.93	2.16	349		-5%	Wading	29	1430	1526	Good		
6	2002-06		K. Faucher	89.0	2.42	215.00	0.92	1.67	205		4%	Wading	27	12:00	13:12	Fair		¢
7	2002-07	8/21/2002	K. Faucher	37.0	0.79	28.40	0.58	0.42	16.6	•	1%	Wading	34	14:21	15:46	Good		
8	2003-01	2/13/2003	L. Cornelius	90.0	2.09	188.00	2.29	2.36	431		-5%	Wading	28	1210	1255	Good		
9	2003-02	2/19/2002	S. Pittman	n/a	n/a	n/a	n/a	4.25	1530		-7%	Indirect	n/a	n/a	n/a	Good		Slope Area No. 1 (WY 2002)
10	2003-03	12/17/2001	S. Pittman	n/a	n/a	n/a	n/a	5.18	2380	ļ	0%	Indirect	n/a	n/a	n/a	Fair		Slope Area No. 2 (WY 2002)
11	2003-04	1/2/2002	S. Pittman	n/a	n/a	n/a	n/a	9.03	7200		7%	Indirect	n/a	n/a	n/a	Fair		Slope Area No. 3 (WY 2002)
12	2003-05	12/16/2002	S. Pittman	n/a	n/a	n/a	n/a	12.71	11600		-9%	Indirect	n/a	n/a	n/a	Poor		Slope Area No. 4 (WY 2003)
													I					
			UTH FC Vater Qu						R					-	IAM N	IATTHEWS Geomorpholog		

			Grah	nam Mat	tthews &	Assoc	ates					
			BARK	ER CREE	EK AT ST	OKELY R	ANCH					
			RATING	TABLE N	IO. 1 Be	egin Date	11/17/01					
											1st	2nd
GH	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09	Diff	Diff
1.1									0	0.28		
1.2	0.55	0.83	1.10	1.38	1.66	1.93	2.21	2.48	2.76	3.03	2.76	
1.3	3.31	3.59	3.86	4.14	4.41	4.69	4.97	5.24	5.52	5.79	2.76	0.00
1.4	6.07	6.34	6.62	6.90	7.17	7.45	7.72	8.00	8.38	8.77	3.10	0.34
1.5	9.17	9.58	10.00	10.40	10.80	11.20	11.70	12.10	12.60	13.00	4.33	1.23
1.6	13.50	13.90	14.30	14.80	15.20	15.70	16.10	16.60	17.00	17.50	4.46	0.13
1.7	18.00	18.40	18.90	19.40	19.90	20.40	20.90	21.40	21.90	22.50	5.04	0.58
1.8	23.00	23.60	24.20	24.90	25.50	26.20	26.80	27.50	28.20	28.80	6.53	1.49
1.9	29.50	30.20	30.90	31.70	32.40	33.10	33.90	34.60	35.40	36.10	7.40	0.87
2	36.9	37.7	38.5	39.3	40.1	41.0	41.8	42.6	43.5	44.3	8.28	0.88
2.1	45.2	46.1	47.0	47.9	48.8	49.7	50.6	51.5	52.5	53.4	9.17	0.89
2.2	54.4	55.3	56.3	57.3	58.3	59.3	60.3	61.3	62.4	63.4	10.10	0.90
2.3	64.4	65.5	66.6	67.6	68.7	69.8	70.9	72.0	73.1	74.3	11.00	0.91
2.4	75.4	76.6	77.7	78.9	80.1	81.2	82.4	83.6	84.8	86.1	11.90	0.92
2.5	87.3	88.5	89.8	91.0	92.3	93.6	94.9	96.2	97.5	98.8	12.80	0.92
2.6	100	101	103	104	106	107	108	110	111	112	13.70	0.93
2.7	114	115	117	118	120	121	123	124	126	127	14.70	0.94
2.8	129	130	132	133	135	136	138	139	141	143	15.60	0.94
2.9	144	146	147	149	151	152	154	156	157	159	16.60	0.95
3	161	163	164	166	168	169	171	173	175	177	17.50	0.96
3.1	178	180	182	184	186	187	189	191	193	195	18.50	0.96
3.2	197	199	201	203	204	206	208	210	212	214	19.50	0.97
3.3	216	218	220	222	224	226	228	230	233	235	20.40	0.97
3.4	237	239	241	243	245	247	249	252	254	256	21.40	0.98
3.5	258	260	263	265	267	269	271	274	276	278	22.40	0.98
3.6	281	283	285	287	290	292	294	297	299	302	23.40	0.99
3.7	304	306	309	311	314	316	318	321	323	326	24.40	0.99
3.8 3.9	328 354	331 356	333 359	336 361	338 364	341 367	343 369	346 372	349 375	351 377	25.40 26.40	1.00 1.00

NOTES: This rating based upon 7 measured discharges in WY 2001, 2002 and 2003. Highest gage height at which a discharge was measured = 2.96 ft.

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

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SOUTH FORK TRINITY RIVER WATERSHED

Suspended Sediment Data Collection Summary for 10 Datalogger Stations

Station	Depth Integrated Samples	Grab samples	Maximum Observed Turbidity (NTU)	Maximum Observed SSC (mg/l)	Maximum Observed Turbidity (NTU)	Maximum Observed SSC (mg/l
BCSR	24	7	110	1100	320	1020
SCWR	22	2	78	290	200	341
BGCH3	24	6	73	375	60	273
HCNH	18	13	100	40	220	403
SCSCG	17	0	29	90	85	307
TCTCR	23	0	36	108	26	89
HCHY	24	8	60	N/A	499	361
SFTFG	17	20	48	106	163	363
ECASFT	4	0	11	23	N/A	N/A
GCASFT	13	0	115	241	245	603
SFTR Watershed Total	611	145				

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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TABLE

		Sample	Numbers and	Maximum N	TU by Water	Year by Site				
SUB-UNIT	SITE NAME	ACRONYM	# SAMPLES WY2001	MAX NTU WY2001	# SAMPLES WY2002	MAX NTU WY2002	# SAMPLES WY2003	MAX NTU WY2003	TOTAL # SAMPLES BY SITE	MAX NTU BY SITE IN PERIOD
Jpper Hayfork	Dubakella Creek	DCWM					3	22	3	22
	Goods Creek	GC36					3	39	3	39
	Potato Creek	PC343	2	45			4	55	6	55
	East Fork Hayfork Creek	EFHC	2	160			3	278	5	278
	Carrier Gulch	CGWR	1	6			3	91	4	91
	Hayfork Creek Arnold Ranch	HCAR	1	14			4	90	5	90
Summit Creek	Summit Creek Summit Creek Rd	SCSCR	3	25	2	55			5	55
	Carr Creek	CCH3	8	24	11	90	4	35	23	90
	Shock Creek	SCAGG	1	20	2	50			3	50
	Gardner Gulch	GGAP	2	13	2	28			4	28
	Duncan Creek	DCSCR	1	7	5	23	4	85	10	85
	Summit Creek Wildwood Rd	SCWR	7	100	13	78	10	450	30	450
Barker	Upper Barker	UBO3			11	38	4	7	15	38
	Little Barker	LBBC			8	18	4	45	12	45
	Barker Trib Barker Valley	BTBV			15	390	12	450	27	450
	Barker Trib Stokely Ranch	BTSR	2	40	5	80	11	600	16	600
	Barker Creek Stokely Ranch Barker Creek Highway 3	BCSR BCH3	3	19 290	13 10	103 279	14 13	320 1000	30 31	320 1000
	· · · ·		-							
layfork Valley	Big Creek	BGCH3	8	10	12	73	10	60	30	73
	Philpot Creek	PCCG	1	7			3	14	4	14
	Salt Creek	SCSG	3	85	10	29	7	85 27	20	85 36
	Tule Creek CG Hyampom Rd D/S	TCTCR CGHR	3	36	11 6	36 45	12	140	23	36 140
	CG New Country Lane U/S	CGNCL	3	6	6	28	7	24	16	28
	Hayfork Creek Hayfork	HCNH	5		8	100	17	215	25	215
laufadi Uuamuam	Little Creek	LCHR			10	39	2	17	12	39
Hayfork-Hyampom Road	No Name at Nine Mile Bridge	NN9MB			7	18	2	8	9	18
loau	Grassy Flats	GCHR			5	21	2	47	7	47
	Big Canyon Creek	BCHR			4	6	1	4	5	6
	Olsen Creek	OCOCR	2	4	16	43	4	37	22	43
	Hayfork Creek at Hyampom	HCHY			9	60	23	800	32	800
Rattlesnake	Upper Rattlesnake Hwy 36	UR36			9	25	9	99	18	99
	Upper Rattlesnake Rd 29N73	UR73			9	11	8	51	17	51
	WF SF Rattlesnake	WFSFR			8	12	2	13	10	13
	SF Rattlesnake	SFR57			8	12	2	16	10	16
	Post Creek	PCH36	1	10	9	26	10	72	20	72
	Little Rattlesnake	LRGS	2	3		40	5	26	7	26
	NF Rattlesnake Rattlesnake Creek	NFR14 RC29	2	5 7	5 6	18 19	10 12	85 103	17 20	85 103
orest Glen	Glen Creek	GGGR	2	1	5	22	8	41	15	41
	SF Trinity Forest Glen	SFTFG			13	48	16	162	29	162
lyampom	Butter Creek	BUCSFT			8	22	3	100	11	100
	Pelletreau Creek	PCHR			14	1300	3	291	17	1300
	Kerlin Creek	KCHR	2	19	21	75	3	73	26	75
	Eltapom Creek	ECASFT	2	2	4	11	-	605	4	11
	SF Trinity below Hyampom USGS	SFTH	2	3	8	220	3	605	13	605
ower Watershed	Grouse Creek	GCASFT			9	115	7	650	16	650
	Madden Creek	MCR6			4	41			4	41
	SF Highway 299				2	144			2	144
OTAL TURBIDITY S	AMPLES		72		343		294		709	
MAXIMUM NTU BY W			12	290	545	1300	2.54	1000	103	1300

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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SOUTH FORK TRINITY RIVER WATERSHED WY 2002-2003 Regression Equations and r² Values by Station

Station	SSC vs. T		T vs. Q		SSC vs. Q		SSL vs. Q	
	y =	r²	y =	r²	y =	r ²	y =	r ²
BCSR	3.565x + 7.894	0.80	0.6845x ^{0.9163}	0.55	0.0835x ^{1.6443}	0.79	2.2525E ⁻⁰⁴ x ^{2.6443}	0.90
SCWR	2.373x - 14.87	0.78	0.1472x ^{0.9201}	0.58	9.192E-03x ^{1.484}	0.74	2.479E-05x ^{2.484}	0.89
BGCH3	1.9497x ^{1.2256}	0.96	NA		NA		3E-06x ^{2.9007}	0.94
HCNH	2.247x + 34.84	0.94	0.01246x ^{1.0254}	0.61	0.4071x ^{0.7574}	0.56	1.098E ⁻⁰³ x ^{1.757}	0.87
SCSG	1.0152x ^{1.2663}	0.72	NA		NA		5E-10x ^{3.7891}	0.98
TCTCR	2.974x - 7.941	0.90	0.0135x ^{1.1571}	0.85	5.926E-04x ^{1.780}	0.91	1.598E-06x ^{2.8}	0.96
HCHY	2.987x - 1.906	0.96	4.051E ⁻⁰⁴ x ^{1.407}	0.81	7.009E- ^{0.5} x ^{1.721}	0.78	1.890E ^{-0.7} x ^{2.721}	0.89
SFTFG	1.008x ^{1.338}	0.88	1.553E ^{-0.3} x ^{1.203}	0.82	3.966E ^{-0.4} x ^{1.465}	0.80	1.070E ^{-0.6} x ^{2.465}	0.92
ECASFT	1.0016x ^{1.3379}	0.86	NA		NA		0.0001x ^{2.1422}	0.76
GCASFT	1.337x ^{1.167}	0.88	0.0419x ^{1.071}	0.50	3.365E-03x ^{1.626}	0.74	9.076E-06x ^{2.626}	0.88

SSC = suspended sediment concentration (mg/l), T = turbidity (NTU), Q = discharge (cfs), SSL = suspended sediment load (tons/day)

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project	GMA GRAHAM MATTHEWS & ASSOCIATES Hydrology • Geomorphology • Stream Restoration P.O. Box 1516 Weaverville, CA 96093-1516
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TABLE

8

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

SOUTH FORK TRINITY RIVER WATERSHED **Total Suspended Sediment Yield For 10 Continuous Recording Stations** WY 2002 WY 2003 Suspended Suspended SSLPA* **SSLPA** Watershed **Sediment Load Sediment Load** Area (mi²) (tons) (tons/mi²) (tons) (tons/mi²) Station BCSR 9.26 54 1,320 498 143 SCWR 28.26 712 25 1,540 54 BGCH3 27.26 1,500 55 2,000 73 HCNH 265.10 36,800 139 211 56.000 SCSG 53.59 N/A N/A 4,000 75 TCTCR 20.25 453 22 684 34 5** HCHY 378.77 1990** 60,500 160 SFTFG 207.58 8,650 42 19,300 93 83*** ECASFT 19.59 347 18 4** GCASFT 53.18 13,500 254 64,000 1,200

* Suspended Sediment Load Per Watershed Area

** partial water year

***December 11-28 only

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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TABLE

SITE	Length of Thalweg Profile (ft)	# of Surveyed Cross Sections	# of Pebble Counts (n=100)	# of Photos Taken	# of Pools Measured for V*	# of Gaged Cross Sections for Slope Area	# of Permanent Benchmarks
ICNH	5110	7	10	39	7	7	3
UCSFT	646	6	7	26	6	4	2
CASFT	3700	4	5	21	8	3	3
CHY	5220	5	10	14	9	4	2
CHR	2510	7	14	22	N/A *	N/A *	2
FTFG	4830	7	13	20	6	5	3
	*	Reach attributes did not	meet criteria for inc	licated method			

								RIVER WATERSH							
		1		Pebble	e Count Si	ze Paramete	ers For Geor	norphic Referenc	e Reaches	s (Fall 2002	2)				
- ··															
Geomorphic	Cross		Sampled	_		meter (mm)	_	Geomorphic	Cross		Sampled		ize Parame		_
Reach	Section	Station	Feature	D ₉₀	D ₈₄	D ₅₀	D _{mean}	Reach	Section	Station	Feature	D ₉₀	D ₈₄	D ₅₀	D _{mean}
BUCSET	1	59-69	wc	173	140	22.0	60.7	GCASFT	1	89-99	LB	55.8	46.1	13.1	22.3
50C3F1		82-87	LB	75.6		34.8	43.0	GCASET		2 68-78	B	160	130	69.7	83.1
		38-43	WC		138	21.5	64.9			36-46	AC	82.9	70.0	37.7	44.5
		25-30	WC	165 189	130	21.5	64.9 78.5			34-45	MCB	61.6	53.7	25.5	44.5 30.6
		14-26	LB	208	157	39.4	76.5			17-23	WC	14.6	12.2	25.5	8.13
		4-9							4	17-23	VVC	14.6	12.2	7.40	6.13
	-		LB	56.6		18.4	26.0 52.7	CETEC		47.57	0.0	20.0	00.7	47.4	10.0
	6	90-100	LØ	144	112	24.4	5Z.1	SFTFG		47-57	SB	32.0 90.0	28.7	17.4	19.6
		17.57			174					72-82	WC		81.0	54.4	57.5
ICHY		47-57	В	220	171	58.3	92.3			2 72-83	LB	46.0	39.0	22.5	25.7
		59-69	В	66.7	56.8	29.0	33.7			20-30	WC	108	87.7	47.3	55.4
		88-98	AC	103	81.1	39.0	47.2		-	82-92	WC	123	106	54.6	63.1
		68-73	MCB	128	86.9	48.6	61.9		-	100-105	WC	27.3	24.9	14.9	19.3
	-	48-53	MCB	NA	50.1	2.18	30.2			38-48	AC	214	171	73.5	94.9
		71-81	AC	151	115	44.4	64.4			74-84	WC	120	100	60.9	70.2
		47-57	В	63.1	54.2	23.3	30.9		-	6 40-50	LB	29.9	26.5	17.1	18.2
		114-124	AC	257	180	41.1	99.0			5 134-139	WC	24.5	21.1	11.6	13.7
		21-31	LB	40.3	34.4	21.0	27.5			32-42	WC	41.9	32.2	16.4	20.3
	5	60-70	WC	38.4	31.0	13.5	20.1		7	61-71	MCB	67.2	58.4	31.5	37.3
		400.470		400	447	50.5	CO O	DOUD	L	5.40	1.0	424	400	27.0	54.0
ICNH		168-178	LB	136		56.5	68.9	PCHR	1	5-10	LB	134	102	37.9	51.0
		226-236	LB	93.8		42.6	47.8		1	54-64	LB	97.7	78.2	30.4	50.3
		93-103	WC	140		56.5	70.1			20-35	WC	148	116	41.8	62.7
	-	148-158	LB	70.8		27.7	33.6		_	2 59-69	LB	49.8	37.7	16.7	24.3
	-	70-80	LB	142		65.1	74.4		-	48-60	WC	160	140	91.0	93.8
		19-20	Lobe	67.3	57.7	43.0	39.9		-	3 70-75	LB	90.0	78.0	33.9	45.6
		60-70	LB	46.0		18.8	22.5			36-46	WC	132	110	49.1	60.4
	-	45-60	LB	51.0		24.0	27.5			110-120	SC	174	132	38.1	63.6
	-	90-95	MCB	69.3	56.2	22.1	30.6		-	28-38	AC	186	147	47.7	74.3
	7	60-70	LB	56.9	48.9	25.2	27.7			57-67	LB	74.8	67.1	29.6	37.2
										66-76	LB	19.4	17.3	5.9	8.90
eature Types:	AC		nel, not wet at t	ime of samp	le				-	89-99	AC	129	110	53.8	61.8
	LB	lateral bar								53-63	LB	31.1	26.4	12.1	15.7
	Lobe	small alluvial			В	bar			7	363-373	AC	119	107	69.4	73.4
	SB	submerged l			SC	secondary cha									
	WC	wetted char	nel		MCB	mid-channel ba	r	Pebble counts utilize	d a modified (portable samp	ling frame with	0.5 ft. interc	epts		
								Sample size ≥ 100 fe							
								Italics: estimated fro	m the distribut	tion					

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

GMA GRAHAM MATTHEWS & ASSOCIATES Hydrology • Geomorphology • Stream Restoration P.O. Box 1516 Weaverville, CA 96093-1516 (530) 623-5327 ph (530) 623-5328 fax TABLE

MAINSTEM S.F.TRINITY BULK SAMPLE DATA

Site	Mean Permeability	Surface		Count			Bulk Sa	-		
	(cm/hr)		mm)	-		rface (mm			Surface (m	
		D ₉₀	D ₈₄	D ₅₀	D ₉₀	D ₈₄	D ₅₀	D ₉₀	D ₈₄	D ₅₀
					1					
SFTFG	2800	60.7	55.9	41.2	65.0	60.5	40.0	66.0	54.0	15.0
					<u> </u>					
SFTHR	2023	67.5	57.8	30.9	85.5	77.0	37.0	45.0	31.0	9.7
						-				
SFTEC	4096	95.5	82.1	29.7	101	87.0	34.5	70.5	54.0	12.0
	4000	55.5	02.1	20.1		07.0	04.0	10.0	04.0	12.0
	SOUTH FORK T Water Quality M					Hydrol P.O.	AM MATTHI ogy • Geomorph Box 1516 Wear	E WS & ASSO(nology • Stream F verville, CA 960	Restoration 93-1516	тае 1
TI	RINITY COUNTY RESOURCE	E CONSERVAT	TION DIS	FRICT		(530) 623-5327 p	h (530) 623-532	8 fax	

USFS SHASTA-TRINITY NATIONAL FOREST SFMU

2002 Temperature Data Site Summary Table

Sort by Alpha

Site Location	Map #	# of days measured	Maximum Daily Average (°F)	Maximum Temp (°F)	7-Day Running Maximum Average (°F)
Bear Creek	5	147	61.1	63.7	62.7
	5 17	147	-		-
Big Creek at Bridge	17 22	154	61.7	64.2	63.3
Butter Creek at 2N10 Bridge			61.5	63.7	62.7
Butter Creek at McCaslin's	23	159	62.9	65.7	65.0
Dubakella Creek	18	159	61.6	64.9	63.7
East Fork Hayfork Creek	19	147	67.0	68.9	67.8
East Fork South Fork Trinity	34	159	62.6	67.0	66.3
Eltapom Creek at 4N09 Bridge	1	144	60.6	63.4	61.8
Eltapom Creek near mouth	2	130	65.8	67.4	66.7
Glen Creek near HWY 36	24	146	61.2	62.8	62.0
Hayfork at Hyampom	6	130	76.8	84.6	83.4
Hayfork Creek at Arnold Ranch	20	147	73.2	80.6	77.8
Hayfork Creek below Bear	7	147	74.4	82.3	80.1
Hayfork Creek below Miners	8	126	75.4	79.1	78.2
Miners Creek	10	143	62.2	65.2	64.3
Naufus Creek	25	74	66.4	0.08	77.3
Pelletreau Creek	3	63	70.7	83.8	80.4
Philpot Creek	11	147	62.6	65.0	63.7
Plummer Creek	26	134	65.9	69.3	68.5
Post Creek	27	146	64.7	71.3	70.1
Potato Creek	21	147	65.1	69.2	68.1
Powell Creek	35	159	63.0	65.5	64.5
Rattlesnake Creek near FG station	29	146	67.5	71.6	70.3
Shell Mtn.Creek	36	145	66.8	72.2	70.7
Silver Creek	37	144	64.6	67.0	66.3
Smokey Creek	38	140	66.0	70.2	69.2
South Fork Trinity above Powell	39	159	62.9	68.1	66.8
South Fork Trinity above Shell	40	145	68.4	79.0	77.1
South ForkTrinity at Concrete Bridge	42	159	73.8	76.9	76.2
South Fork Trinity above Smokey	41	144	68.5	72.3	71.3
South Fork Trinity at Forest Glen	31	127	72.0	76.1	75.4
South Fork Trinity above Plummer	30	134	73.8	76.9	76.2
South Fork Trinity at Hyampom	32	70	75.6	78.7	77.6
South Fork Trinity below Slide	4	130	73.3	79.6	78.2

Source: USFS

Sites/temps with 7-day Maximum Average > 68.4°F (20°C) Sites/temps with 7-day Maximum Average < 68.4°F (20°C)

SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

GMA

GRAHAM MATTHEWS & ASSOCIATES

Hydrology • Geomorphology • Stream Restoration P.O. Box 1516 Weaverville, CA 96093-1516 (530) 623-5327 ph (530) 623-5328 fax TABLE

SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT DISTRIBUTION OF PRIVATE/PUBLIC LAND OWNERSHIP BY STUDY WATERSHED

	SITE	PRIVATE	PERCENT	PUBLIC	PERCENT	WATERSHED
STUDY SITE WATERSHED	ACRONYM	OWNERSHIP (acres)	TOTAL AREA	OWNERSHIP (acres)	TOTAL AREA	AREA (acres)
Barker Creek at Hwy 3	BCH3	2,011.2	30.9%	4,500.6	69.1%	6,511
Bear Creek above Hayfork Creek	BCHC	153.9	3.2%	4,731.1	96.8%	4,885
Big Canyon Cr. at Hyampom Rd.	BCHR	1,165.3	100.0%			1,165
Barker Creek at Stokley Ranch	BCSR	1,902.4	29.7%	4,500.5	70.3%	6,403
Big Creek at Hwy 3	BGCH3	1,693.0	9.7%	15,755.9	90.3%	17,449
Barker Trib. at Barker Valley Rd.	BTBV	9.0	100.0%			9
Barker Trib. At Stokely Ranch	BTSR	10.9	100.0%			11
Butter Creek above SF Trinity	BUCSFT	860.9	3.7%	22,230.7	96.3%	23,092
Carr Creek at Hwy 3	CCH3	2,581.5	67.6%	1,234.7	32.4%	3,816
Duncan Creek at Summit Creek Rd.	DCSCR	1,767.1	42.7%	2,372.1	57.3%	4,139
Eltapom Creek above South Fork Trinity	ECASFT	1,114.8	8.9%	11,425.2	91.1%	12,540
Grouse Creek above SF Trinity	GCASFT	13,678.9	40.2%	20,358.1	59.8%	34,037
Grassy Flats at Hyampom Rd.	GCHR	4.7	0.3%	1,376.6	99.7%	1,381
Gardner Gulch above Pond	GGAP	782.0	96.4%	29.0	3.6%	811
Hayfork Creek near Hyampom	HCHY	49,599.7	20.5%	192,775.0	79.5%	242,415
Hayfork Creek near Hayfork	HCNH	42,389.7	25.0%	127,231.2	75.0%	169,661
Kerlin Creek at South Fork Road	KCSFR	1,241.0	49.0%	1,293.7	51.0%	2,535
Little Barker at Barker Cr. Rd.	LBBC	180.3	13.6%	1,146.6	86.4%	1,327
Little Creek at Hyampom Rd.	LCHR	6.1	0.1%	5,811.3	99.9%	5,817
Madden Ck @ Route 6	MCR6	1,640.8	11.4%	12,777.6	88.6%	14,419
No Name at 9 Mile Bridge.	NN9MB	1,706.6	100.0%			1,707
Olsen Creek at Olsen Creek Rd.	OCOCR	268.1	6.5%	3,826.3	93.5%	4,094
Pelletreau Creek at South Fork Rd.	PCSFT	5,608.4	74.2%	1,945.4	25.8%	7,554
Shock Creek above Gardner Gulch	SCAGG	812.6	82.7%	169.5	17.3%	982
Summit Creek at Summit Creek Rd.	SCSCR	1,269.4	78.3%	352.6	21.7%	1,622
Salt Ck. @ Salt Cr. Growers	SCSG	3,608.6	10.5%	30,692.1	89.5%	34,301
Summit Creek at Wildwood Rd.	SCWR	12,063.9	66.7%	6,019.6	33.3%	18,083
South Fork Rattlesnake at 29N57	SFR57	1,267.9	100.0%			1,268
So. Fork Trinity at Sandy Bar	SFSB	105,997.8	17.8%	489,783.4	82.2%	595,900
South Fork Trinity at Forest Glen	SFTFG	7,561.3	5.7%	125,245.7	94.3%	132,852
Tule Creek @ Tule Creek Road	TCTCR	402.5	3.1%	12,554.9	96.9%	12,957
Upper Barker at USFS 32N03	UB03	513.2	15.0%	2,914.0	85.0%	3,427
Upper Rattlesnake ab Hwy 36 Water Hole	UR36	101.6	1.1%	9,157.1	98.9%	9,259
Upper Rattlesnake above 29N73	UR73	25.8	0.6%	4,291.0	99.4%	4,317
W. Fork of S. Fork Rattlesnake at 29N57	WFSFR	970.4	100.0%	,		970
TOTAL FOR WATERSHED		105.997.8	17.8%	489.783.4	82.2%	595,900

Notes: GIS Data combined from various sources

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

TABLE

GMA 💳

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			ACRES OF IN	DICATED SL	OPE CLASS			TOTA
LOCATION	0-20%	20-30%	30-40%	40-50%	50-60%	60-70%	> 70%	(acres
SFSB	109.014.8	106.639.5	120.060.5	99.238.5	72,327.5	46.640.7	41.871.0	595.79
BUCSFT	7,653.6	5,350.0	4,238.7	2,719.8	1,599.0	850.4	679.8	23,09
ECASFT	2,410.6	2,507.0	2,586.4	1,932.1	1,259.6	781.8	1.061.3	12.53
GCASFT	2,247.0	5,723.5	8,862.5	7,008.7	4,868.0	2,936.6	2,383.7	34.03
KCSFR	472.9	709.5	589.1	338.5	183.9	100.9	140.1	2.53
MCR6	1,484.7	1,615.8	1,989.3	2,315.8	2,434.8	2,173.4	2.403.4	14.41
OCOCR	748.6	714.3	742.5	700.5	593.1	350.1	245.3	4.09
PCSFR	1,053.3	1,974.1	1,817.0	1,220.2	758.0	412.4	319.1	7,55
HCHY			43,337.3	42.581.5	34,503,1		16.624.3	
	47,341.3	35,780.5				22,188.9		242,35
BCHC	191.4	261.2	605.2	1,055.8	1,240.0	920.6	610.4	4,88
BCHR	31.3	36.3	113.7	265.1	309.7	232.1	177.1	1,16
GCHR	269.4	255.2	251.5	207.5	164.5	120.0	113.2	1,38
LCHR	271.0	370.9	777.3	1,150.4	1,353.6	1,093.9	800.2	5,81
NN9MB	57.0	85.3	219.3	352.1	412.7	339.9	240.6	1,70
HCNH	38,912.9	28,163.5	32.382.4	28,756.9	20,837.2	12,235.6	8.323.6	169,61
BGCH3	2,312.4	1,476.8	2,478.4	3,237.8	3,430.5	2,603.4	1,902.1	17.44
SCSG	8,311.2	7,508.7	7.349.9	5,227.9	3,203.0	1,659.2	1,040.8	34.30
TCTCR	2.604.9	2,755.0	2,879.3	2,198.5	1.294.8	723.7	501.0	12,95
BCH3	1,377.7	940.3	1,294.3	1,279.4	924.4	452.5	240.7	6,50
BTSR	3.2	1.6	1.8	1.5	0.9	1.0	0.9	
BTBV	1.6	1.5	1.8	1.4	0.8	1.0	0.9	
BCSR	1,331.0	919.8	1,277.5	1,270.3	917.8	447.4	236.4	6,40
LBBC	70.9	119.3	259.3	367.9	304.8	141.0	62.9	1,32
UB03	298.1	549.7	832.6	783.1	541.2	269.9	151.4	3,42
SCWR	3,409.5	2,106.0	2,835.3	3,385.1	3,006.8	1,923.8	1,408.6	18,07
CCH3	287.4	440.5	810.5	948.8	724.3	380.3	222.4	3,81
DCSCR	631.4	381.3	510.8	755.9	822.8	580.5	456.6	4,13
GGAP	34.4	34.9	86.6	153.8	196.8	175.1	129.4	81
SCAGG	72.7	69.4	88.0	152.4	223.5	197.6	178.3	98
SCSCR	249.3	282.4	298.5	303.2	243.3	142.8	98.2	1,61
SFTFG	21,249.1	28,519.7	33,109.6	23,828.0	13.658.7	7,023.8	5,441.0	132.82
UR36		and the second se	and the second se		730.4	344.9	5,441.0	9,25
SFR57	2,123.1	2,275.6	2,185.6	1,400.0		66.0	45.5	
	207.0	264.4	325.9	231.0	128.1			1,20
UR73 WFSFR	1,178.7	1,162.6	979.8	571.3 198.4	267.2	110.7 68.2	46.4	4,31
WFORK	121.9	175.8	251.7	198.4	120.1	08.2	34.5	9
nationalist	1	PERCENTW	ATCOCUED	ADEA OF INI				
	0.0001					OPE CLASS	> 700/	
LOCATION	0-20%	20-30%	30-40%	40-50%	50-60%	60-70%	> 70%	
SFSB	0-20% 18.3%						> 70% 7.0%	>50%
		20-30%	30-40%	40-50%	50-60%	60-70%		>50%
SFSB	18.3%	20-30% 17.9%	30-40% 20.2%	40-50% 16.7%	50-60% 12.1%	60-70% 7.8%	7.0%	>50% 21
SFSB BUCSFT	18.3% 33.1%	20-30% 17.9% 23.2%	30-40% 20.2% 18.4%	40-50% 16.7% 11.8%	50-60% 12.1% 6.9%	60-70% 7.8% 3.7%	7.0% 2.9%	>50% 21 11 24
SFSB BUCSFT ECASFT	18.3% 33.1% 19.2%	20-30% 17.9% 23.2% 20.0%	30-40% 20.2% 18.4% 20.6%	40-50% 16.7% 11.8% 15.4%	50-60% 12.1% 6.9% 10.0%	60-70% 7.8% 3.7% 6.2%	7.0% 2.9% 8.5%	>50% 21 13 24 29
SFSB BUCSFT ECASFT GCASFT KCSFR	18.3% 33.1% 19.2% 6.6% 18.7%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0%	7.0% 2.9% 8.5% 7.0% 5.5%	>50%
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6	18.3% 33.1% 19.2% 6.6% 18.7% 10.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7%	>50% 21 11 24 29 16 48
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8% 18.1%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0%	>50%
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8% 18.1% 24.1%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2%	>50%
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 19.5%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8% 18.1%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2%	60-70% 7.8% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9%	>50% 2: 1: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2:
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8% 18.1% 24.1%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2%	>509 2: 1: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2:
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR HCHY	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 19.5%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8%	30-40% 20.2% 18.4% 20.6% 26.0% 23.2% 13.8% 18.1% 24.1% 17.9%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2%	60-70% 7.8% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9%	>509 21 11 24 25 10 40 40 40 25 30 30 56
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR HCHY BCHC	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 19.5% 3.9%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 5.3%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2% 25.4%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9% 12.5%	>509 21 11 24 29 10 40 40 40 29 29 10 10 10 10 10 50 6
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR BCHC BCHR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 19.5% 3.9% 2.7%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 17.4% 26.1% 14.8% 5.3% 3.1%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7%	50-60% 12.1% 6.9% 10.0% 14.3% 16.9% 14.5% 10.0% 14.2% 25.4% 26.6%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9% 12.5% 15.2%	>50% 21 13 24 24 16 44 25 15 30 56 6 26
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR BCHC BCHR BCHR GCHR	18.3% 33.1% 19.2% 6.6% 18.7% 18.3% 13.9% 19.5% 3.9% 2.7% 19.5%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 5.3% 3.1% 18.5%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7% 15.0%	50-60% 12.1% 6.9% 10.0% 14.3% 16.9% 14.5% 10.0% 14.5% 25.4% 26.6% 11.9%	60-70% 7.8% 3.7% 6.2% 8.6% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 8.7%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9% 6.9% 12.5% 15.2% 8.2%	>50% 21 13 24 16 44 25 16 44 25 33 56 6 6 55
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR HCHY BCHC BCHR BCHR GCHR LCHR NN9MB	18.3% 33.1% 19.2% 6.6% 18.7% 18.3% 13.9% 13.9% 2.7% 2.7% 2.7% 4.7% 3.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 26.1% 14.8% 5.3% 3.1% 6.4% 5.0%	30-40% 20.2% 18.4% 20.6% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 13.4% 13.4% 12.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7% 15.0% 19.8% 20.6%	50-60% 12.1% 6.9% 10.0% 14.3% 14.3% 14.5% 14.5% 10.0% 14.2% 25.4% 26.6% 26.6% 21.9% 23.3% 24.2%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 8.7% 18.8% 19.9%	7.0% 2.9% 8.5% 7.0% 5.5% 6.0% 4.2% 6.9% 12.5% 12.5% 8.2% 13.8% 14.1%	>50% 21 13 24 25 26 16 48 26 15 56 66 66 66 55 55
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR BCHY BCHC BCHR BCHR CCHR LCHR NN9MB	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 19.5% 3.9% 2.7% 19.5% 3.3% 2.7% 3.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 17.4% 17.4% 16.5% 14.8% 5.3% 14.8% 5.3% 14.5% 0.4% 5.0% 16.6%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2% 13.4% 13.4% 12.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.6% 21.6% 22.7% 15.0% 19.8% 20.6% 17.0%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2% 25.4% 26.6% 11.9% 23.3% 24.2%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 9.2% 18.8% 19.9% 8.7% 18.8% 19.9% 7.2%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 6.9% 12.5% 15.2% 8.2% 13.8% 14.1% 4.9%	>50% 21 13 24 25 16 44 44 45 56 66 66 66 66 56 56 56 20 20 20 20 20 20 20 20 20 20 20 20 20
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR BCHC BCHR BCHR BCHR LCHR NN9MB HCNH BGCH3	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 2.7% 19.5% 4.7% 3.3% 2.2.9% 13.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 14.8% 5.3% 3.1% 18.5% 6.4% 6.4% 5.0% 16.6% 8.5%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2% 13.4% 13.4% 13.4% 12.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7% 19.8% 19.8% 10.6% 17.0% 18.6%	50-60% 12.1% 6.9% 10.0% 14.3% 16.9% 14.5% 10.0% 14.2% 25.4% 26.6% 11.9% 23.3% 24.2% 12.3% 19.7%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 8.7% 18.8% 19.9% 7.2% 14.9%	7.0% 2.9% 8.5% 7.0% 6.0% 4.2% 6.9% 12.5% 15.2% 8.2% 13.8% 14.1% 4.9% 10.9%	>50% 22 13 24 24 24 24 25 25 30 56 56 55 55 55 24 24 44
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR HCHY BCHC BCHR GCHR LCHR NN9MB HCNH BGCH3 SCSG	18.3% 33.1% 19.2% 6.6% 18.7% 18.3% 13.9% 19.5% 3.9% 2.7% 19.5% 4.7% 3.3% 22.9% 13.3% 22.9%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 26.1% 14.8% 5.3% 3.1% 14.8% 5.3% 6.4% 5.0% 18.5% 21.9%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2% 13.4% 12.8% 19.1% 14.2% 21.4%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7% 19.8% 20.6% 15.0% 19.8% 20.6% 15.4% 16.1% 16.2% 17.6% 15.6% 15.4% 15.4% 15.4% 16.2% 15.4% 15.4% 16.4% 15.4% 15.4% 15.4% 15.4% 16.2% 15.4% 15.4% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.2% 15.6% 15.6% 15.2% 15.6% 1	50-60% 12.1% 6.9% 10.0% 14.3% 14.5% 10.0% 14.5% 10.0% 14.2% 25.4% 26.6% 26.6% 23.3% 24.2% 11.9% 23.3% 24.2% 19.7% 9.3%	60-70% 7.8% 3.7% 6.2% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 18.8% 19.9% 18.8% 19.9% 14.9% 4.8%	7.0% 2.9% 8.5% 7.0% 5.5% 6.0% 4.2% 6.9% 15.2% 8.2% 13.8% 14.1% 4.9% 10.9% 3.0%	>50% 22 10 24 24 24 24 24 24 10 10 10 10 10 10 10 10 10 10 10 10 10
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR BCHC BCHR BCHR BCHR BCHR LCHR NIN9MB HCNH BGCH3	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 2.7% 19.5% 4.7% 3.3% 2.2.9% 13.3%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 14.8% 5.3% 3.1% 18.5% 6.4% 6.4% 5.0% 16.6% 8.5%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2% 13.4% 13.4% 13.4% 12.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 21.6% 22.7% 19.8% 19.8% 10.6% 17.0% 18.6%	50-60% 12.1% 6.9% 10.0% 14.3% 16.9% 14.5% 10.0% 14.2% 25.4% 26.6% 11.9% 23.3% 24.2% 12.3% 19.7%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 8.7% 18.8% 19.9% 7.2% 14.9%	7.0% 2.9% 8.5% 7.0% 6.0% 4.2% 6.9% 12.5% 15.2% 8.2% 13.8% 14.1% 4.9% 10.9%	>50% 22 10 24 24 24 24 24 24 10 10 10 10 10 10 10 10 10 10 10 10 10
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR HCHY BCHC BCHR GCHR LCHR NN9MB HCNH BGCH3 SCSG	18.3% 33.1% 19.2% 6.6% 18.7% 18.3% 13.9% 19.5% 3.9% 2.7% 19.5% 4.7% 3.3% 22.9% 13.3% 22.9%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 26.1% 14.8% 5.3% 3.1% 14.8% 5.3% 6.4% 5.0% 16.6% 21.9% 21.3%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 13.4% 12.8% 13.4% 12.8% 13.4% 12.8% 13.4% 22.2%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.2% 17.6% 21.6% 22.7% 19.8% 20.6% 15.0% 19.8% 20.6% 15.0% 15.8% 15.2% 17.0%	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 14.5% 10.0% 14.2% 25.4% 26.6% 26.6% 23.3% 24.2% 11.9% 23.3% 24.2% 19.7% 9.3% 10.0%	60-70% 7.8% 3.7% 6.2% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 18.8% 19.9% 18.8% 19.9% 14.9% 4.8% 5.6%	7.0% 2.9% 8.5% 7.0% 5.5% 6.0% 4.2% 12.5% 12.5% 13.8% 14.1% 4.9% 10.9% 3.0% 3.9%	>50% 22 13 24 25 25 26 25 56 56 56 56 56 56 56 24 24 11 11 11 11
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCCCR PCSFR HCHY BCHC BCHR BCHC BCHR LCHR NN9MB HCNH BGCH3 SCSG TCTCR BCH3	18.3% 33.1% 19.2% 6.6% 18.7% 18.3% 13.9% 19.5% 2.7% 4.7% 3.3% 22.9% 13.3% 12.5% 13.3% 22.9% 13.3%	20-30% 17.9% 23.2% 20.0% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 5.3% 3.1% 14.8% 5.3% 16.6% 8.5% 16.6% 8.5% 21.9% 21.3% 14.4%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 24.1% 17.9% 12.4% 9.8% 18.2% 13.4% 12.8% 19.1% 14.2% 22.2% 19.9%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 16.2% 17.6% 21.6% 22.7% 19.8% 20.6% 15.0% 19.8% 20.6% 15.0% 19.8% 20.6% 15.4% 21.6% 22.7% 15.4% 22.7% 15.4% 25.4% 20.6% 25.4% 2	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2% 25.4% 26.6% 11.9% 23.3% 24.2% 12.3% 19.7% 9.3% 10.0%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 7.2% 14.9% 7.2% 14.9% 5.6% 7.0%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 4.2% 4.2% 15.2% 8.2% 13.8% 14.1% 10.9% 10.9% 3.0% 3.9%	>50% 22 13 24 25 25 26 26 56 56 56 56 56 56 24 24 24 24 24 24 24 24 24 24 24 24 24
SFSB BUCSFT ECASFT GCASFT KCSFR MCR6 OCOCR PCSFR PCSFR BCHC BCHR BCHR BCHR LCHR NN9MB HCNH BGCH3 SCSG TCTCR BCH3 BTSR	18.3% 33.1% 19.2% 6.6% 18.7% 10.3% 18.3% 13.9% 2.7% 19.5% 3.3% 2.7% 13.3% 22.9% 13.3% 24.2% 20.1% 20.1% 20.1% 20.0%	20-30% 17.9% 23.2% 20.0% 16.8% 28.0% 11.2% 17.4% 26.1% 14.8% 5.3% 3.1% 14.5% 21.3% 21.3% 14.4% 15.0%	30-40% 20.2% 18.4% 20.6% 23.2% 13.8% 18.1% 14.1% 17.9% 12.4% 19.8% 13.4% 12.8% 19.1% 14.2% 21.4% 21.4% 21.4% 22.2% 19.9% 16.8%	40-50% 16.7% 11.8% 15.4% 20.6% 13.4% 16.1% 17.1% 16.2% 17.6% 22.7% 15.0% 19.8% 20.6% 17.0% 18.6% 15.2% 17.0% 18.6% 17.0% 18.6% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 18.6% 15.2% 17.0% 15.2% 17.0% 15.2% 17.0% 15.2% 1	50-60% 12.1% 6.9% 10.0% 14.3% 7.3% 16.9% 14.5% 10.0% 14.2% 26.6% 11.9% 23.3% 24.2% 12.3% 19.7% 9.3% 10.0% 14.2% 8.4%	60-70% 7.8% 3.7% 6.2% 8.6% 4.0% 15.1% 8.6% 5.5% 9.2% 18.8% 19.9% 8.7% 18.8% 19.9% 7.2% 14.9% 4.8% 5.6% 7.0% 9.1%	7.0% 2.9% 8.5% 7.0% 5.5% 16.7% 6.0% 4.2% 12.5% 15.2% 8.2% 13.8% 14.1% 10.9% 3.0% 3.9% 8.2%	>50% 21 11 22 21 11 11 11 11 33 56 66 66 55 55 55 55 24 44 41 11 11 11 22 22 52 24 24 24 22 25
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SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT

GMA

GRAHAM MATTHEWS & ASSOCIATES

Hydrology • Geomorphology • Stream Restoration P.O. Box 1516 Weaverville, CA 96093-1516 (530) 623-5327 ph (530) 623-5328 fax TABLE

TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

Bear Creek above Hayfork Creek 2001.7 2.883.3 Big Canyon Cr. at Hyampom Rd. 334.1 626.6 204.6 Barker Creek at Stokley Ranch 1.154.8 5247.5 Big Creek at Stokley Ranch 1.056.2 15891.8 Barker Trib. at Barker Valley Rd. 9.0 0.0 Barker Trib. At Stokley Ranch 10.8 0.0 Butter Creek at Hwy 3 113.4 3702.5 Duncan Creek at Summit Creek Rd. 722.2 3417.1 Etapom Creek above South Fork Trinity 1193.1 5.767.7 5571.6 Grause Creek above South Fork Trinity 1193.1 5.767.7 5571.6 Grather Gulch above Pond 9.7 801.2 1381.3 Gardner Gulch above Pond 9.7 8012.2 334.1 6.0	ACRES OF INDICATED GEOLOGIC TERRANE											
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W. FUR UI 3, FUR Returns at 28137 433.0 103.3 333.	3.4	1	970.4									

SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT GEOLOGIC TERRANES BY STUDY WATERSHED

		PERCENT W	ATERSHED AF	REA OF INDICA	TED GEOLOGI	C TERRANE	5 M 1. 2013
STUDY SITE WATERSHED	Alluvial Deposits	Hayfork Terrane	Granitics	Rattlesnake Creek Terrane	Galice Formation	Franciscan Formation	South Fork Mountain Schist
Barker Creek at Hwy 3	19.3%	80.7%					
Bear Creek above Hayfork Creek		41.0%	59.0%		+-		
Big Canyon Cr. at Hyampom Rd.		28.7%	53.8%	17.6%			
Barker Creek at Stokley Ranch	18.0%	82.0%					
Big Creek at Hwy 3	8.9%	91.1%					
Barker Trib. at Barker Valley Rd.	99.6%	0.4%	-				-
Barker Trib. At Stokely Ranch	99.7%	0.3%			**		
Butter Creek above SF Trinity		**	14,7%	84.2%	1.1%		
Carr Creek at Hwy 3	3.0%	97.0%			++		
Duncan Creek at Summit Creek Rd.	17.4%	82.6%					
Eltapom Creek above South Fork Trinity		9.5%	46.0%	44.5%			
Grouse Creek above SF Trinity			8.1%	8.1%	23.8%	42.8%	17.3%
Grassy Flats at Hyampom Rd.				100.0%			
Gardner Gulch above Pond	1.2%	98.8%					
Hayfork Creek near Hyampom	7.4%	45.8%	28.0%	18.1%		0.6%	
Hayfork Creek near Hayfork	10.1%	52.8%	18.8%	17.3%		0.9%	
Kerlin Creek at South Fork Road				20.4%	19.4%		60.2%
Little Barker at Barker Cr. Rd.		100.0%					
Little Creek at Hyampom Rd		87.0%	13.0%				
Madden Ck @ Route 6			23.0%	22.7%	51.0%		3.3%
No Name at 9 Mile Bridge.		5.6%	85.5%	8.8%			
Olsen Creek at Olsen Creek Rd.	6.5%		11.1%	82.3%			
Pelletreau Creek at South Fork Rd.	0.0 /0		11.170	2.5%	44.2%		53.2%
Shock Creek above Gardner Gulch	9.4%	90.6%					00.270
Summit Creek at Summit Creek Rd.	17.1%	82.9%					
Salt Ck. @ Salt Cr. Growers		33.9%	22.6%	40.2%		3.2%	
Summit Creek at Wildwood Rd.	21.3%	78.7%	2.4.010	10.2.10		0.2.10	
South Fork Rattlesnake at 29N57			6.2%	78.0%	15.8%		
So. Fork Trinity at Sandy Bar	3.4%	18.9%	19.1%	28.8%	10.2%	7.9%	11.7%
South Fork Trinity at Forest Glen	0.170	10.070	12.5%	30.4%	9.2%	23.1%	24.8%
Tule Creek @ Tule Creek Road	0.3%	14.2%	31.8%	53.7%	0.2.10		27.070
Upper Barker at USFS 32N03		100.0%	5				
Upper Rattlesnake ab Hwy 36 Water Hole			14.2%	69.9%	15.9%		
Upper Rattlesnake above 29N73			6.3%	93.7%	10.070		
W. Fork of S. Fork Rattlesnake at 29N57		++	44.7%	18.9%	36.4%		
TOTAL FOR WATERSHED	3.41%	18.85%	19.12%	28,75%	10.24%	7.88%	11.74%

Notes: GIS Data combined from various sources

SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT

GMA

GRAHAM MATTHEWS & ASSOCIATES

Hydrology • Geomorphology • Stream Restoration P.O. Box 1516 Weaverville, CA 96093-1516 (530) 623-5327 ph (530) 623-5328 fax TABLE

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TRINITY COUNTY RESOURCE CONSERVATION DISTRICT

													PERCENT
				FIRE	AREAS BY	DECADE	(acres)			1000	FIRE AREA	WATERSHED	BURNED
Study Site Watershed	1910s	1920s	1930s	1940s	1950s	1960s	1970s	1980s	1990s	2000s	TOTAL	TOTAL AREA	1910-2000
Barker Creek at Hwy 3									2.0		2.0	6.511	0.0%
Bear Creek above Hayfork Creek			-		6.4	-					6.4	4,885	0.1%
Big Canyon Cr. at Hyampom Rd.					67.9						67.9	1,165	5.8%
Barker Creek at Stokley Ranch								-	2.0		2.0	6.403	0.0%
Big Creek at Hwy 3					1,340.0						1,340.0	17,449	7.7%
Butter Creek above SF Trinity		2.123.1						10,464.3			12,587.4	23.092	54.5%
Carr Creek at Hwy 3					1				2,518.5		2,518.5	3,816	66.0%
Duncan Creek at Summit Creek Rd.		4.2		129.3		169.6					303.1	4,139	7.3%
Eltapom Creek above South Fork Trinity	298.5							2,511.4			2,809.9	12,540	22.4%
Grouse Creek above SF Trinity	213.6	931.3	1,318.9		1944	303.8			S		2,767.7	34,037	8.1%
Grassy Flats at Hyampom Rd.					-			732.1		-	732.1	1,381	53.0%
Gardner Gulch above Pond						5.7			1.		5.7	811	0.7%
Hayfork Creek near Hyampom		1,826.3		309.8	3,696.2	5,392.7	547.9	13,621.4	6,193.2	1,089.8	32,677.1	242,415	13.5%
Hayfork Creek near Hayfork	-	1,158.4		309.8	1,485.4	5,392.7	547.9	8,373.4	6,193.2	142.6	23,603.3	169,661	13.9%
Little Barker at Barker Cr. Rd.									2.0		2.0	1,327	0.1%
Little Creek at Hyampom Rd.		2.2	· · · · · · · · · · · · · · · · · · ·		1,865.3		S			53.2	1,920.7	5,817	33.0%
Madden Ck @ Route 6			100.5		148.3			1.000			248.8	14,419	1.7%
Olsen Creek at Olsen Creek Rd.	1		1. 1. 1. 1.					2,182.8			2,182.8	4,094	53.3%
Pelletreau Creek at South Fork Rd.								399.0		1	399.0	7,554	5.3%
Summit Creek at Summit Creek Rd.	S					970.2	()				970.2	1,622	59.8%
Salt Ck. @ Salt Cr. Growers		560.8		- 2013	1			4,838.3	678.2		6,077.3	34,301	17.7%
Summit Creek at Wildwood Rd.		4.2		181.3		1,545.1	542.3		4,690.5	10.000	6,963.4	18,083	38.5%
So. Fork Trinity at Sandy Bar	1,785.1	7,239.5	3,490.7	309.8	3,963.6	9,118.1	547.9	68,286.3	6,193.2	1,089.8	102,024.0	595,900	17.1%
South Fork Trinity at Forest Glen		2,052.7	74.8			3,256.2		13,291.0			18,674.7	132,852	14.1%
Tule Creek @ Tule Creek Road								2,550.0			2,550.0	12,957	19.7%
Upper Rattlesnake ab Hwy 36 Water Hole				1	-			6.1			6.1	9,259	0.1%
TOTAL FOR WATERSHED BY DECADE	1,785.1	7,239.5	3,490.7	309.8	3,963.6	9,118.1	547.9	68,286.3	6,193.2	1,089.8	102,024.0		
% OF TOTAL PERIOD	1.7%	7.1%	3.4%	0.3%	3.9%	8.9%	0.5%	66.9%	6.1%	1.1%	100.0%		

FIRE AREAS BY DECADE BY SUB-WATERSHED, 1910-2000

and the second sec	100 C		PERC	ENT WAT	ERSHED A	REA BUR	NED BY DE	ECADE		
Study Site Watershed	1910s	1920s	1930s	1940s	1950s	1960s	1970s	1980s	1990s	2000s
Barker Creek at Hwy 3		-							0.0%	
Bear Creek above Hayfork Creek					0.1%		-		-	
Big Canyon Cr. at Hyampom Rd.					5.8%				-	
Barker Creek at Stokley Ranch								-	0.0%	
Big Creek at Hwy 3					7.7%		-	-	-	
Butter Creek above SF Trinity		9.2%						45.3%		
Carr Creek at Hwy 3	-				-			-	66.0%	-
Duncan Creek at Summit Creek Rd.		0.1%		3.1%		4.1%	-	-	-	
Eltapom Creek above South Fork Trinity	2.4%			-				20.0%		
Grouse Creek above SF Trinity	0.6%	2.7%	3.9%			0.9%		-		
Grassy Flats at Hyampom Rd.					-			53.0%		
Gardner Gulch above Pond				-	+	0.7%		+		
Hayfork Creek near Hyampom	-	0.8%	0.0%	0.1%	1.5%	2.2%	0.2%	5.6%	2.6%	0.4%
Hayfork Creek near Hayfork	-	0.7%	0.0%	0.2%	0.9%	3.2%	0.3%	4.9%	3.7%	0.1%
Little Barker at Barker Cr. Rd.						-		-	0.1%	
Little Creek at Hyampom Rd.	-	0.0%	-	÷	32.1%	-	-	-	-	0.0
Madden Ck @ Route 6			0.7%		1.0%		-	-	-	
Olsen Creek at Olsen Creek Rd.								53.3%		
Pelletreau Creek at South Fork Rd.	-	-				-	-	5.3%	-	
Summit Creek at Summit Creek Rd.	-	-	-	-	-	59.8%	-	-	-	-
Salt Ck. @ Salt Cr. Growers		1.6%						14.1%	2.0%	
Summit Creek at Wildwood Rd.		0.0%		1.0%		8.5%	3.0%	-	25.9%	
So. Fork Trinity at Sandy Bar	0.3%	1.2%	0.6%	0.1%	0.7%	1.5%	0.1%	11.5%	1.0%	0.2%
South Fork Trinity at Forest Glen		1.5%	0.1%	+	-	2.5%	-	10.0%		
Tule Creek @ Tule Creek Road						-		19.7%		
Upper Rattlesnake ab Hwy 36 Water Hole	-	-		•		+	•	0.1%	+	-

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT AMOUNT OF TIMBER HARVEST BY STUDY WATERSHED FROM 1970 TO PRESENT

	SITE	NUMBER OF	HARVEST TOTAL	WATERSHED	PERCENT
STUDY SITE WATERSHED	ACRONYM	HARVEST UNITS	1970-Present (acres)	AREA (acres)	HARVESTED
				. ,	
Barker Creek at Hwy 3	BCH3	86	517.8	6,511	7.95%
Bear Creek above Hayfork Creek	BCHC	7	191.4	4,885	3.92%
Big Canyon Cr. at Hyampom Rd.	BCHR	32	152.9	1,165	13.13%
Barker Creek at Stokley Ranch	BCSR	86	517.8	6,403	8.09%
Big Creek at Hwy 3	BGCH3	194	1,801.4	17,449	10.32%
Butter Creek above SF Trinity	BUCSFT	307	5,109.4	23,092	22.13%
Carr Creek at Hwy 3	CCH3	8	2,167.3	3,816	56.79%
Duncan Creek at Summit Creek Rd.	DCSCR	11	1,083.3	4,139	26.17%
Eltapom Creek above South Fork Trinity	ECASFT	128	1,620.8	12,540	12.93%
Grouse Creek above SF Trinity	GCASFT	397	8,700.0	34,037	25.56%
Grassy Flats at Hyampom Rd.	GCHR	16	98.3	1,381	7.11%
Gardner Gulch above Pond	GGAP	5	765.2	811	94.36%
Hayfork Creek near Hyampom	HCHY	1701	33,325.5	242,415	13.75%
Hayfork Creek near Hayfork	HCNH	1156	28,012.5	169,661	16.51%
Kerlin Creek at South Fork Road	KCSFR	35	879.7	2,535	34.70%
Little Barker at Barker Cr. Rd.	LBBC	8	34.3	1,327	2.58%
Little Creek at Hyampom Rd.	LCHR	44	397.2	5,817	6.83%
Madden Ck @ Route 6	MCR6	116	3,360.5	14,419	23.31%
No Name at 9 Mile Bridge.	NN9MB	38	114.0	1,707	6.68%
Olsen Creek at Olsen Creek Rd.	OCOCR	70	782.5	4,094	19.11%
Pelletreau Creek at South Fork Rd.	PCSFT	32	811.3	7,554	10.74%
Shock Creek above Gardner Gulch	SCAGG	3	675.7	982	68.81%
Summit Creek at Summit Creek Rd.	SCSCR	3	49.7	1,622	3.06%
Salt Ck. @ Salt Cr. Growers	SCSG	203	3,882.1	34,301	11.32%
Summit Creek at Wildwood Rd.	SCWR	58	6,736.7	18,083	37.25%
South Fork Rattlesnake at 29N57	SFR57	11	94.9	1,268	7.48%
So. Fork Trinity at Sandy Bar	SFSB	4391	89,478.6	595,900	15.02%
South Fork Trinity at Forest Glen	SFTFG	827	14,811.9	132,852	11.15%
Tule Creek @ Tule Creek Road	TCTCR	273	1,946.2	12,957	15.02%
Upper Barker at USFS 32N03	UB03	73	391.2	3,427	11.41%
Upper Rattlesnake ab Hwy 36 Water Hole	UR36	89	725.9	9,259	7.84%
Upper Rattlesnake above 29N73	UR73	25	271.5	4,317	6.29%
W. Fork of S. Fork Rattlesnake at 29N57	WFSFR	14	105.0	970	10.83%
TOTAL FOR WATERSHED		4391	- 89,478.6	595,900	15.02%

Notes: Data combined from USFS files and aerial photo analysis

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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TABLE

	MILE	S OF ROADS O	F INDICATED	ГҮРЕ	WATERSHED	DRAINAGE	ROAD DENSITY
STUDY SITE WATERSHED	NATIVE	ROCKED	PAVED	HIGHWAY	ROAD TOTAL (mi)	AREA (mi ²)	(mi/mi ²)
Barker Creek at Hwy 3	34.8	10.0			44.8	10.17	4.40
Bear Creek above Hayfork Creek	8.3				8.3	7.63	1.08
Big Canyon Cr. at Hyampom Rd.	6.9	1.2			8.0	1.82	4.42
Barker Creek at Stokley Ranch	34.3	10.0			44.3	10.00	4.42
Big Creek at Hwy 3	76.3	9.3	10.4	0.1	96.2	27.26	3.53
Barker Trib. at Barker Valley Rd.					-	0.01	0.00
Barker Trib. At Stokely Ranch	0.1				0.1	0.02	3.25
Butter Creek above SF Trinity	119.2	38.4	6.3		163.9	36.08	4.54
Carr Creek at Hwy 3	29.7	0.7			30.3	5.96	5.09
Duncan Creek at Summit Creek Rd.	20.7				20.7	6.47	3.20
Eltapom Creek above South Fork Trinity	38.5	14.1	10.7		63.4	19.59	3.24
Grouse Creek above SF Trinity	176.5	45.9	10.5		232.8	53.18	4.38
Grassy Flats at Hyampom Rd.	3.9	1.6			5.5	2.16	2.54
Gardner Gulch above Pond	7.1				7.1	1.27	5.59
Hayfork Creek near Hyampom	954.7	156.8	95.1	37.1	1,243.6	378.77	3.28
Hayfork Creek near Hayfork	760.1	108.5	75.2	37.1	980.8	265.10	3.70
Kerlin Creek at South Fork Road	19.5	2.8	0.0		22.4	3.96	5.65
Little Barker at Barker Cr. Rd.	4.8	0.1			4.9	2.07	2.36
Little Creek at Hyampom Rd.	22.5	0.1			22.6	9.09	2.48
Madden Ck @ Route 6	25.5	16.5	8.4		50.5	22.53	2.24
No Name at 9 Mile Bridge.	6.5	4.7	0.0		11.3	2.67	4.23
Olsen Creek at Olsen Creek Rd.	17.0	7.3	2.5		26.8	6.40	4.19
Pelletreau Creek at South Fork Rd.	35.8	2.3	3.0		41.1	11.80	3.48
Shock Creek above Gardner Gulch	6.1				6.1	1.53	3.99
Summit Creek at Summit Creek Rd.	10.5			2.4	12.9	2.53	5.11
Salt Ck. @ Salt Cr. Growers	130.3	18.8	1.9	18.0	169.0	53.59	3.15
Summit Creek at Wildwood Rd.	118.5	2.0	0.1	7.0	127.6	28.26	4.52
South Fork Rattlesnake at 29N57	4.2	5.9	-		10.1	1.98	5.12
So. Fork Trinity at Sandy Bar	2,282.8	503.9	195.2	52.8	3,034.7	931.09	3.26
South Fork Trinity at Forest Glen	507.3	104.2	20.9	8.9	641.3	207.58	3.09
Tule Creek @ Tule Creek Road	53.1	18.5	4.9		76.4	20.25	3.77
Upper Barker at USFS 32N03	18.2	7.8			26.0	5.36	4.85
Upper Rattlesnake ab Hwy 36 Water Hole	40.9	19.9		5.2	65.9	14.47	4.56
Upper Rattlesnake above 29N73	19.1	7.3		1.9	28.2	6.74	4.19
W. Fork of S. Fork Rattlesnake at 29N57	4.7	3.4			8.1	1.52	5.33
	0.000.0	500.0	405.0	50.0	0.004.7	004.00	2.00
TOTAL FOR WATERSHED	2,282.8	503.9	195.2	52.8	3,034.7	931.09	3.26

SOUTH FORK TRINITY RIVER WATER QUALITY MONITORING PROJECT MILES OF ROAD TYPES AND ROAD DENSITY BY STUDY WATERSHED

Notes: GIS Data combined from various sources

SOUTH FORK TRINITY RIVER Water Quality Monitoring Project

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						וח	SCH	ARG	F SU	мма	RY S	HEET	-						
														0000					
		L	LOCATION: Ba		Barker Trib. at		at Barker Vall						WA		EAR:	2002,	2003		
leasurement	WY	Date	Made By:	Width	Mean	Area	Mean	Gage	Discharge	Rating		Method	No. of Msmt	Begin	End	Mamt	Recorder	Notes	
Number	Momt #			(feet)	Depth (feet)	(ft²)	Velocity (ft/sec)	Height (feet)	(cfs)	Shift Adj.	Percent Diff.		sections	Time (hours)	Time (hours)	Rating	level	GH correction = + 6	5'
1	2002-01	11/26/2001	S. Pittman	7.0	0.23	1.61	0.38	1.75	0.61			Wading	19	1616	1647	Good		gravel bar control may be s	shifty
2	2002-02 2002-03	1/20/2002	S. Pittman	0.5	0.40	0.45	0.50	1.64	0.16			Catch	<u> </u>	4545	4500	Fair		culvert = 1.175 gal/s	
3 4	2002-03	3/5/2002 2/17/2003	K. Faucher	2.5 3.7	0.18	0.45	0.53	1.64	0.24			Wading	9 8	1515	1530	Fair			
4 5	2003-01	3/16/2003	L. Cornelius	3.7 9.6	0.18 0.29	0.68 2.74	1.66 1.11	1.90 2.05	1.13 3.03			Wading Wading	8 24	1140 932	1150 951	Fair Good			
6	2003-02	4/29/2003	L. Cornelius	9.0 10.0	0.29	5.10	2.33	2.05	11.90			Wading	24	711	732	Good			
•	2000 00	472372003	E. Concido	10.0	0.01	0.10	2.00	2.24	11.00			Waang	24		152	0000			
								2.38	23.80									Rating Curve Extension	
7	2003-04		S. Pittman		•	•		4.76	53.00	••••••		synthetic		•		poor		17% of BCSR 12/16/02 pe	ak
8	2003-05		S. Pittman	•				3.66	31.62			synthetic				poor		17% of BCSR 12/15/02 ob	serve
																		-	
														A -				T	AB
		SO	UTH FC	RK	TRI	NITY	Y RI	VER					GRA		латт	HFWS	& 155	OCIATES	AB
		V	Vater Qua	ality I	Monit	oring	Proj	ect					Hyd	rology •	Geomo	rphology	• Strea	m Restoration	7
	T	RINITY CO	MINITV DE	SOUD		NICED	оллатт		бари	T			P			eavervil 7 ph (53		96093-1516 5328 fax	20

BARKER CREEK WATERSHED Total Suspended Sediment Yield

2.07 5.36	14	7				
			57	27	13	
5.30	57	/ 11	126	120	22	68 152
9.26	498	54	258	1324	143	311
10.17	835	82	318	2404	236	383
						65
						71
H FORK TRI				GMA GRAHAM MATTH Hydrology • Geomor	IEWS & ASSOCIATE	
	0.57 0.63	0.57 107 0.63 258	0.57 107 188 0.63 258 410	0.57 107 188 54 0.63 258 410 59 * Suspended Sedir	0.57 107 188 54 285 0.63 258 410 59 618 * Suspended Sediment Load Per Water	0.57 107 188 54 285 500 0.63 258 410 59 618 981 * Suspended Sediment Load Per Watershed Area





WATER QUALITY MONITORING PROJECT

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Steel gage house contour-mounted to downstream side of tree on Eltapom Creek.



Steel gage house mounted to 4x6 posts in concrete: South Fork Trinity at Forest Glen.

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FIGURE



GMA gage built atop the excavated USGS (11528500) Hayfork Creek near Hyampom gage.



Close-up of the old USGS stilling well and inside staff plate for the Hayfork Creek near Hyampom Gage.

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FIGURE



Tule Creek near bankfull stage during the December 14-16, 2002 storm.



Salt Creek during the December 14-16, 2002 storm. White circle shows location of gage intake.

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Story board to the left of body indicates: Cross Section 1, left bank (HCNH).



Left bank Cross Section 5 (HCHY), showing slope-area crest gage for recording flood peaks.

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FIGURE



GMA benchmark: aluminum capped 5/8 in. rebar in concrete (HCNH BM #2).



USGS Reference Mark near the Hayfork Creek in Hyampom Gage.

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Residual pool volume (V*) soundings along transect near South Fork Trinity at Forest Glen.



Pebble count sampling grid on Grouse Creek mid-channel bar, Cross Section 4.

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FIGURE



Bulk sampling of mainstem spawning gravels along a surveyed cross section (SFTEC).



24 inch McNeil sampler and backpack mounted permeability pump on the mainstem at Hyampom Road.

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Example of hand-drawn Discharge Rating Curve: Hayfork Creek near Hyampom. Circles indicate direct discharge measurements (meter), triangles indicate indirect discharge measurements (slope-area method).

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Confluence of Barker Creek and Hayfork Creek during the December, 16 2002 storm, well below the peak.

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FIGURE

32













EVALUATION OF THE EFFECTS OF RIPARIAN GRAZING ON TURBIDITY



CEDAR GULCH


































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SOUTH FORK TRINITY RIVER

WATER QUALITY MONITORING PROJECT, WY2001-2003

80

80 L 0

100

STATION (ft)

120

140

GMA =

160

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180

200

APPENDIX

G-10



APPENDIX

G-12

























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APPENDIX

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